



Geoid Determination by FFT Techniques

Michael G. Sideris
sideris@ucalgary.ca

Department of Geomatics Engineering
University of Calgary

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Matching the gravimetric geoid to the GPS-levelling undulations

Georgia Fotopoulos (gfotopou@ucalgary.ca)

Dept. of Geomatics Engineering, University of Calgary



Introduction: Geoid Determination by the Remove-Restore Technique

Stokes's Boundary Value Problem

Problem definition

$$\nabla^2 T = \frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} = 0$$

$$\frac{\partial T}{\partial r} + \frac{2}{r}T + \Delta g = 0$$

Solution

$$T = \frac{R}{4\pi} \iint_{\sigma} \Delta g S(\psi) d\sigma \quad \Rightarrow \quad N = \frac{T}{\gamma}$$

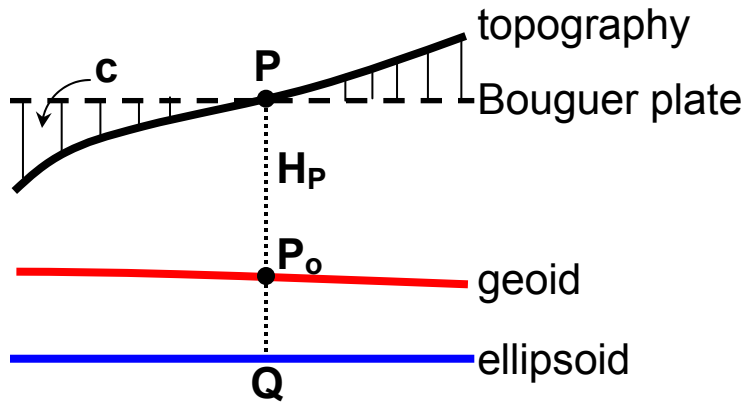
Gravity anomalies given on the geoid

(no masses outside the boundary surface)

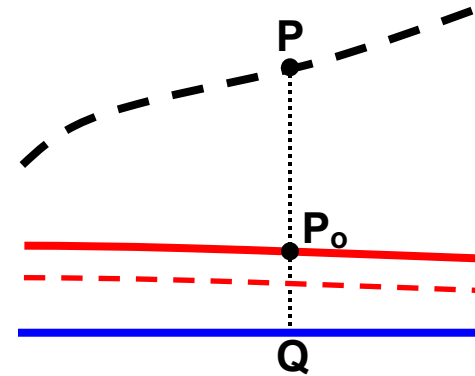
Terrain reductions

Terrain Reductions

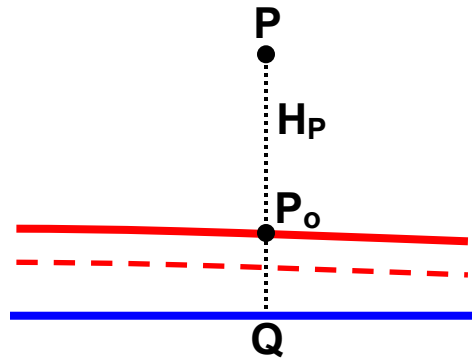
(example: Helmert's Condensation)



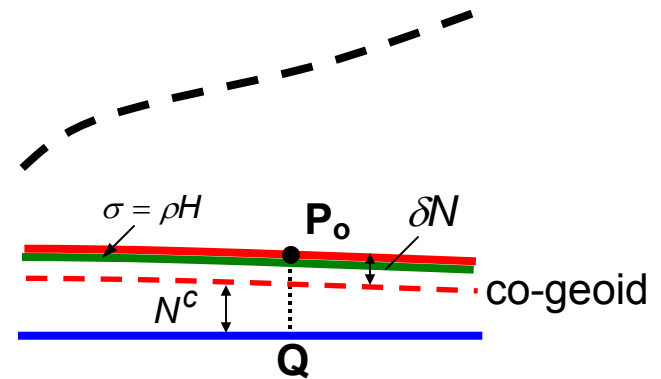
$$\Delta g_P = g_P - \gamma_Q$$



$$\Delta g'_P = \Delta g_P - A_P = \Delta g_P - BC + c$$



$$\Delta g'_{P_0} = \Delta g'_P + F$$



$$\begin{aligned} \Delta g_{P_0} &= \Delta g'_P + F + A_{P_0}^c = \Delta g_P + F + c \\ &= \Delta g_P^{FA} + c = \Delta g_{Faye} \end{aligned}$$

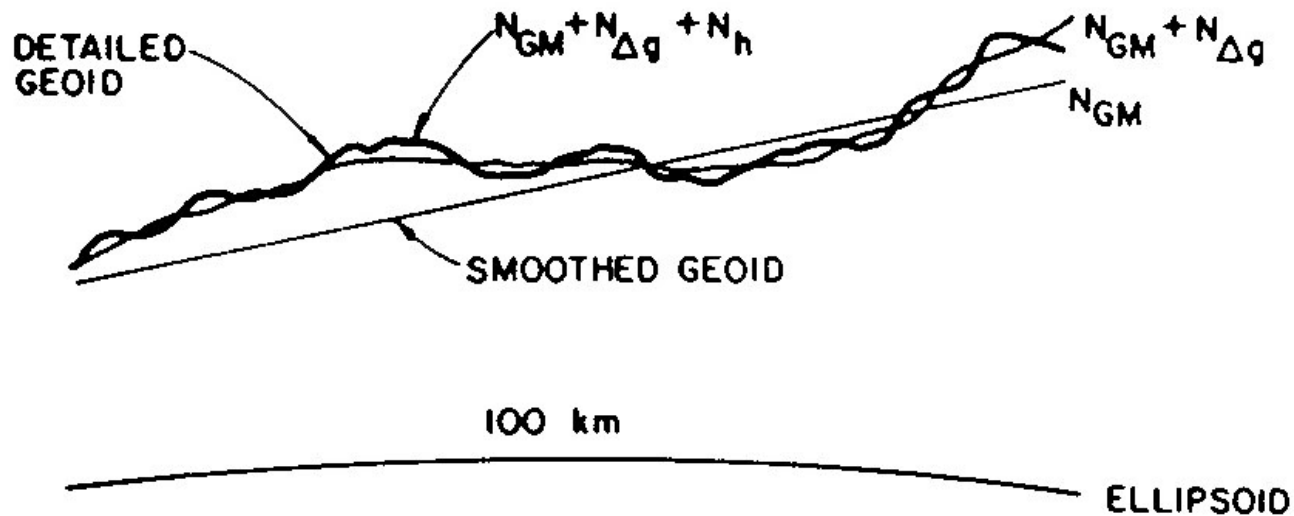
The Remove-Restore Technique

Separate the different frequency contributions

- GM (long wavelengths)
- local gravity data (medium wavelengths)
- DTM (short wavelengths)

$$\Delta g = \Delta g^{FA} - \Delta g^{GM} - \Delta g^H$$

$$N = N^{GM} + N^{\Delta g} + N^H$$



Basic Equations

GM-contributions, in spherical approximation

$$\Delta g_P^{GM} = G \sum_{n=2}^{n_{\max}} (n-1) \sum_{m=0}^n [C_{nm} \cos m\lambda_P + S_{nm} \sin m\lambda_P] P_{nm}(\sin \varphi_P)$$

$$N_P^{GM} = R \sum_{n=2}^{n_{\max}} \sum_{m=0}^n [C_{nm} \cos m\lambda_P + S_{nm} \sin m\lambda_P] P_{nm}(\sin \varphi_P)$$

Δg -contributions, in planar approximation

$$N_P^{\Delta g} = \frac{1}{2\pi\gamma} \iint_E \frac{\Delta g}{l} dx dy, \quad l = [(x - x_P)^2 + (y - y_P)^2]^{1/2}$$

H-contributions, in planar approximation

$$\delta A_P = c_P = -\Delta g_P^H \approx \frac{1}{2} k\rho \iint_E \frac{(H - H_P)^2}{l^3} dx dy$$

$$\delta N_P \approx -\frac{\pi k\rho}{\gamma} H_P^2 - \frac{k\rho}{6\gamma} \iint_E \frac{H^3 - H_P^3}{l^3} dx dy$$

Why Use FFT?

- FFT provides very fast evaluation of convolution sums/integrals with gridded data
- In planar approximation, the Stokes and terrain correction integrals are convolutions
- In spherical approximation, these integrals are convolutions along the parallels, and so are the summations for the GM-contributions
- Gravity and topography data are usually provided on regular grids
- Computations for very large areas can be performed on a PC



The Fourier Transform and its Properties

Real Sinusoids

$$s(t) = A_0 \cos(\omega_0 t + \phi_0) :$$

Sinusoid of frequency ω_0

A_0 *amplitude*

ω_0 *cyclic frequency*

t *time (or distance)*

ϕ_0 *phase angle*

Expansion 

$$s(t) = a \cos \omega_0 t + b \sin \omega_0 t$$

where

$$a = A_0 \cos \phi_0, \quad b = -A_0 \sin \phi_0$$

$$A_0 = (a^2 + b^2)^{1/2}$$

$$\phi_0 = \arctan\left(\frac{-b}{a}\right)$$

$$\omega_0 = \frac{2\pi}{T_0} = 2\pi f_0$$

T_0 *period*

f_0 *frequency*

Sinusoids in complex form

$$s_c(t) = a \cos \omega_0 t \pm i a \sin \omega_0 t = a e^{\pm i \omega_0 t}$$

Real sinusoids in complex form

$$s(t) = A_0 \cos(\omega_0 t + \phi_0) =$$

$$A_0 \frac{e^{i(\omega_0 t + \phi_0)} + e^{-i(\omega_0 t + \phi_0)}}{2} = \frac{A_0}{2} e^{i\phi_0} e^{i\omega_0 t} + \frac{A_0}{2} e^{-i\phi_0} e^{-i\omega_0 t}$$

Fourier Series

If $g(t) = g(t + T)$; $\int_0^T g(t) dt = \int_{t_0}^{t_0+T} g(t) dt$, then

$$g(t) = \sum_{n=0}^{\infty} \left(a_n \cos \frac{2\pi n}{T} t + b_n \sin \frac{2\pi n}{T} t \right)$$

$$a_n = \frac{2}{T} \int_{t_0}^{t_0+T} g(t) \cos nt \, dt; \quad b_n = \frac{2}{T} \int_{t_0}^{t_0+T} g(t) \sin nt \, dt$$

Provided that: $g(t)$ has a finite numbers of maxima and minima in a period and a finite number of finite discontinuities (Dirichlet's conditions)

Complex form

$$g(t) = \frac{1}{T} \sum_{n=-\infty}^{\infty} G_n e^{i\omega_n t}, \quad \omega_n = \frac{2\pi n}{T}$$

$$G_n = \int_{-T/2}^{T/2} g(t) e^{-i\omega_n t} dt, \quad G_n = \frac{1}{2} (a_n - ib_n), \quad n = 0, \pm 1, \pm 2, \dots$$

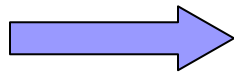
$$\text{Call } \Delta\omega = \frac{2\pi}{T} \Rightarrow \begin{cases} \omega_n = n\Delta\omega \\ \frac{1}{T} = \frac{\Delta\omega}{2\pi} \end{cases} \Rightarrow g(t) = \sum_{n=-\infty}^{\infty} \frac{G_n}{2\pi} e^{i\omega_n t} \Delta\omega$$

The Continuous Fourier Transform

$$g(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} G(\omega) e^{i\omega t} d\omega \Rightarrow \text{Inverse CFT}$$

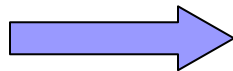
$$G(\omega) = \int_{-\infty}^{\infty} g(t) e^{-i\omega t} dt \Rightarrow \text{Direct CFT}$$

Since $\omega = 2\pi f$



$$g(t) = \int_{-\infty}^{\infty} G(f) e^{i2\pi ft} df = F^{-1}\{G(f)\}$$
$$G(f) = \int_{-\infty}^{\infty} g(t) e^{-i2\pi ft} dt = F\{g(t)\}$$

$G(f)$ is complex



$$G(f) = G_R(f) + iG_I(f) = |G(f)| e^{i\theta(f)}$$

$$\text{Amplitude} \Rightarrow |G(f)| = \left[G_R^2(f) + G_I^2(f) \right]^{1/2}$$

$$\text{Phase angle} \Rightarrow \theta(f) = \text{Arg}\{G(f)\} = \arctan \frac{G_I(f)}{G_R(f)}$$

The CTF (continued)

Conditions for Existence :

- The integral of $|g(t)|$ from $-\infty$ to $+\infty$ exists (it is $< \infty$)
- $g(t)$ has only finite discontinuities
- If $g(t)$ is periodic or impulse, $G(f)$ does not exist

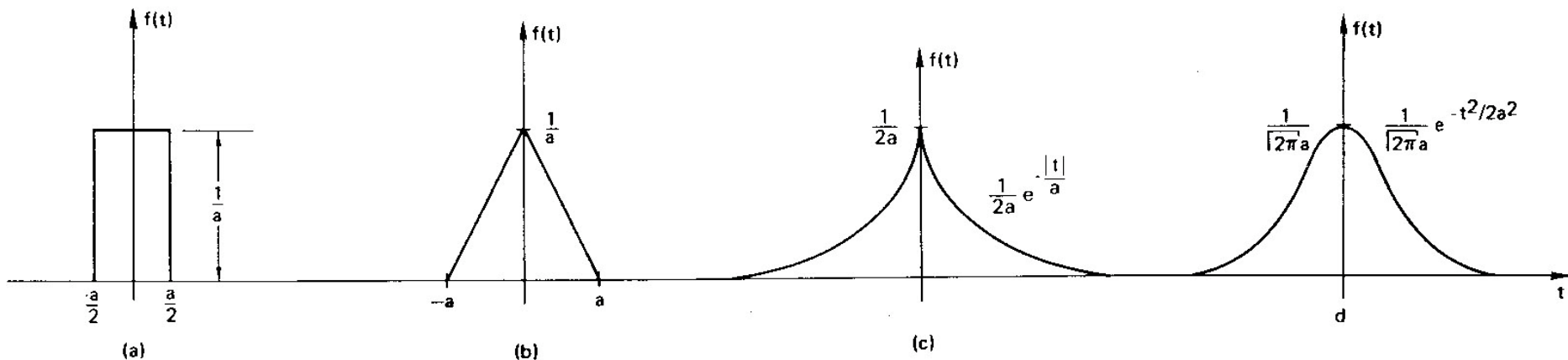
The Impulse Function

Definition :

$$\left. \begin{array}{l} \delta(t - t_0) = 0, \quad t \neq t_0 \\ \int_{-\infty}^{\infty} \delta(t - t_0) dt = 1 \end{array} \right\} \Leftrightarrow \delta(t) = \lim_{a \rightarrow 0} f(t, a)$$

Definition as a distribution

$$\int_{-\infty}^{\infty} \delta(t - t_0) \phi(t) dt = \phi(t_0)$$



The Impulse Function (continued)

Definition as a generalized limit :

$$\text{If } \lim_{n \rightarrow \infty} \int_{-\infty}^{\infty} f_n(t) \phi(t) dt = \phi(0) \quad \Rightarrow \quad \delta(t) = \lim_{n \rightarrow \infty} f_n(t)$$

Properties :

$$\delta(t_0)h(t) = h(t_0)\delta(t_0)$$

$$\delta(at) = |a|^{-1} \delta(t)$$

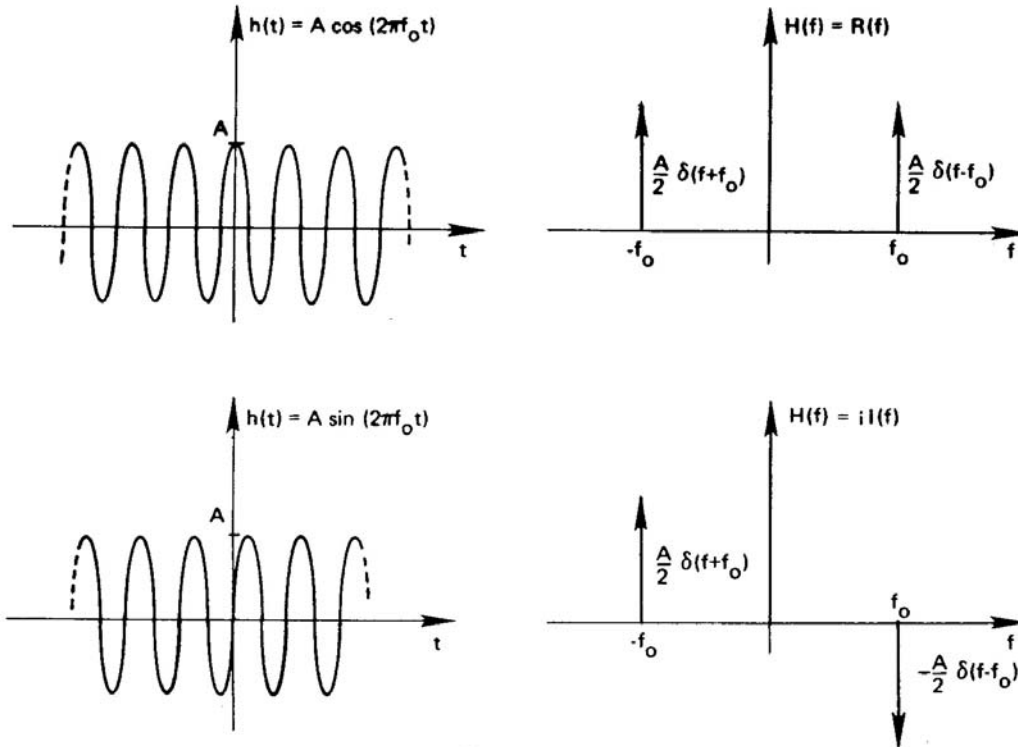
$$F\{K\delta(t)\} = K$$

e.g. If we define it as $\delta(t) = \lim_{a \rightarrow \infty} \frac{\sin at}{\pi t}$,

$$\text{then } \int_{-\infty}^{\infty} \cos(2\pi ft) df = \int_{-\infty}^{\infty} e^{i2\pi ft} df = \delta(t)$$

Used, as a distribution, for the (otherwise nonexistent) CFT of periodic functions

The CTF of cosine and sine



$$A \cos(2\pi f_0 t) \leftrightarrow \frac{A}{2} \delta(f - f_0) + \frac{A}{2} \delta(f + f_0)$$

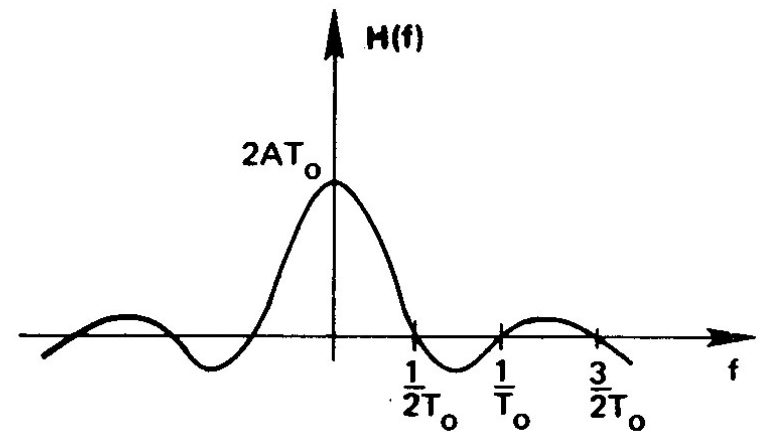
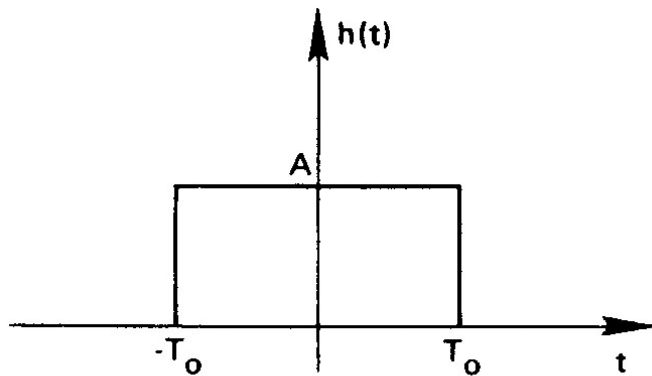
$$A \sin(2\pi f_0 t) \leftrightarrow i \frac{A}{2} \delta(f + f_0) - i \frac{A}{2} \delta(f - f_0)$$

The Sampling Function

$$III(t) = \sum_{n=-\infty}^{\infty} \delta(t - nT) \leftrightarrow F\{III(t)\} = \frac{1}{T} \sum_{n=-\infty}^{\infty} \delta\left(f - \frac{n}{T}\right)$$

$$III(t)f(t) = \sum_{n=-\infty}^{\infty} f(nT)\delta(t - nT) \Rightarrow \text{Digitization}$$

The Rectangle and sinc Functions



$$h(t) = \begin{cases} A, & |t| < T_0/2 \\ A/2, & t = \pm T_0/2 \\ 0, & |t| > T_0/2 \end{cases} \leftrightarrow H(f) = 2AT_0 \text{sinc}(2T_0 f),$$

$$\text{sinc}(f) = \frac{\sin(\pi f)}{\pi f}$$

Properties of the CFT

- Linearity $ah(t) + bg(t) \leftrightarrow aH(f) + bG(f)$
- Symmetry $H(t) \leftrightarrow h(-f)$
- Time scaling $h(at) \leftrightarrow \frac{1}{|a|} H\left(\frac{f}{a}\right)$
- Time shifting $h(t - t_o) \leftrightarrow H(f)e^{-i2\pi ft_o}$
- Differentiation $\frac{\partial^n h(t)}{\partial t^n} \leftrightarrow (i2\pi f)^n H(f)$
- Integration $\int_{-\infty}^t h(x) dx \leftrightarrow \frac{1}{i2\pi f} H(f) + \frac{1}{2} H(0) \delta(f)$

Properties of the CFT (continued)

- DC-value $\int_{-\infty}^{\infty} h(t) dt = H(0)$
- Even function $h_E(t) \leftrightarrow H_E(f) = R_E(f)$
- Odd function $h_O(t) \leftrightarrow H_O(f) = iI_O(f)$
- Real function $h(t) = h_R(t) \leftrightarrow H(f) = R_E(f) + iI_O(f)$
- Imaginary function $h(t) = ih_I(t) \leftrightarrow H(f) = R_O(f) + iI_E(f)$

Convolution and Correlation

$$x(t) = \int_{-\infty}^{\infty} g(t')h(t-t')dt' = g(t) * h(t) = h(t) * g(t) = \int_{-\infty}^{\infty} h(t')g(t-t')dt'$$

$$y(t) = \int_{-\infty}^{\infty} g(t')h(t+t')dt' = g(t) \otimes h(t) \neq h(t) \otimes g(t)$$

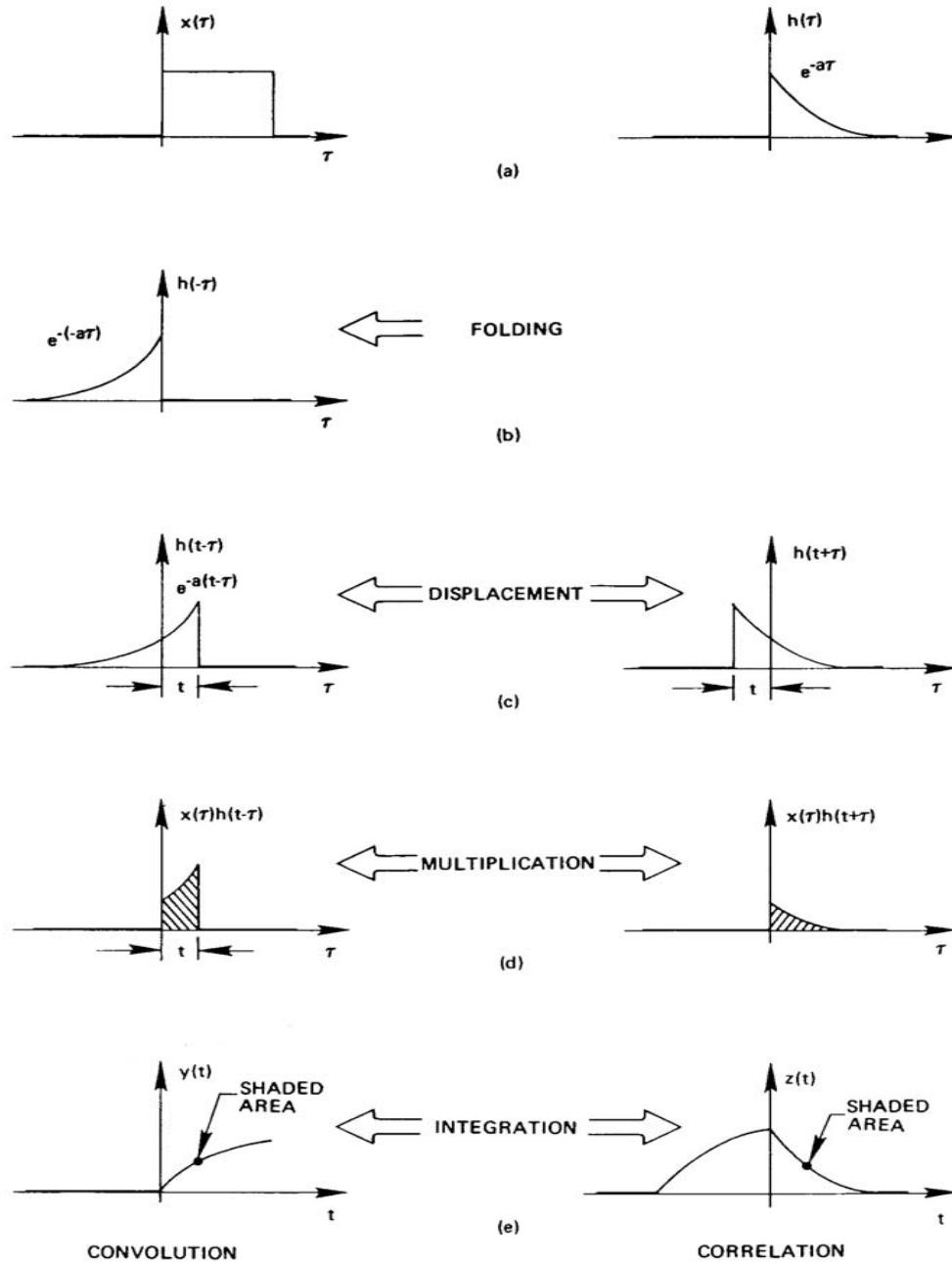
Convolution theorem

$$X(f) = \mathbf{F}\{g(t) * h(t)\} = \mathbf{F}\{g(t)\}\mathbf{F}\{h(t)\} = G(f)H(f)$$

Correlation theorem

$$Y(f) = \mathbf{F}\{g(t) \otimes h(t)\} = G(f)H^*(f)$$

Pictorial Representation of Convolution and Correlation



Convolution and Correlation (continued)

Properties :

a) If either $g(t)$ or $h(t)$ is even, then $g(t) * h(t) = g(t) \otimes h(t)$

b) $\delta(t + \tau) * h(t) = h(t + \tau)$, $\delta(t) * h(t) = h(t)$

c) $x'(t) = (g(t) * h(t))' = g'(t) * h(t) = g(t) * h'(t)$

d) $F\{h(t)g(t)\} = F\{h(t)\} * F\{g(t)\} = H(f) * G(f)$

e) If $h(t)$ and $g(t)$ are time limited functions, i.e, non – zero in the domain $-T_0 \leq t \leq T_0$, then

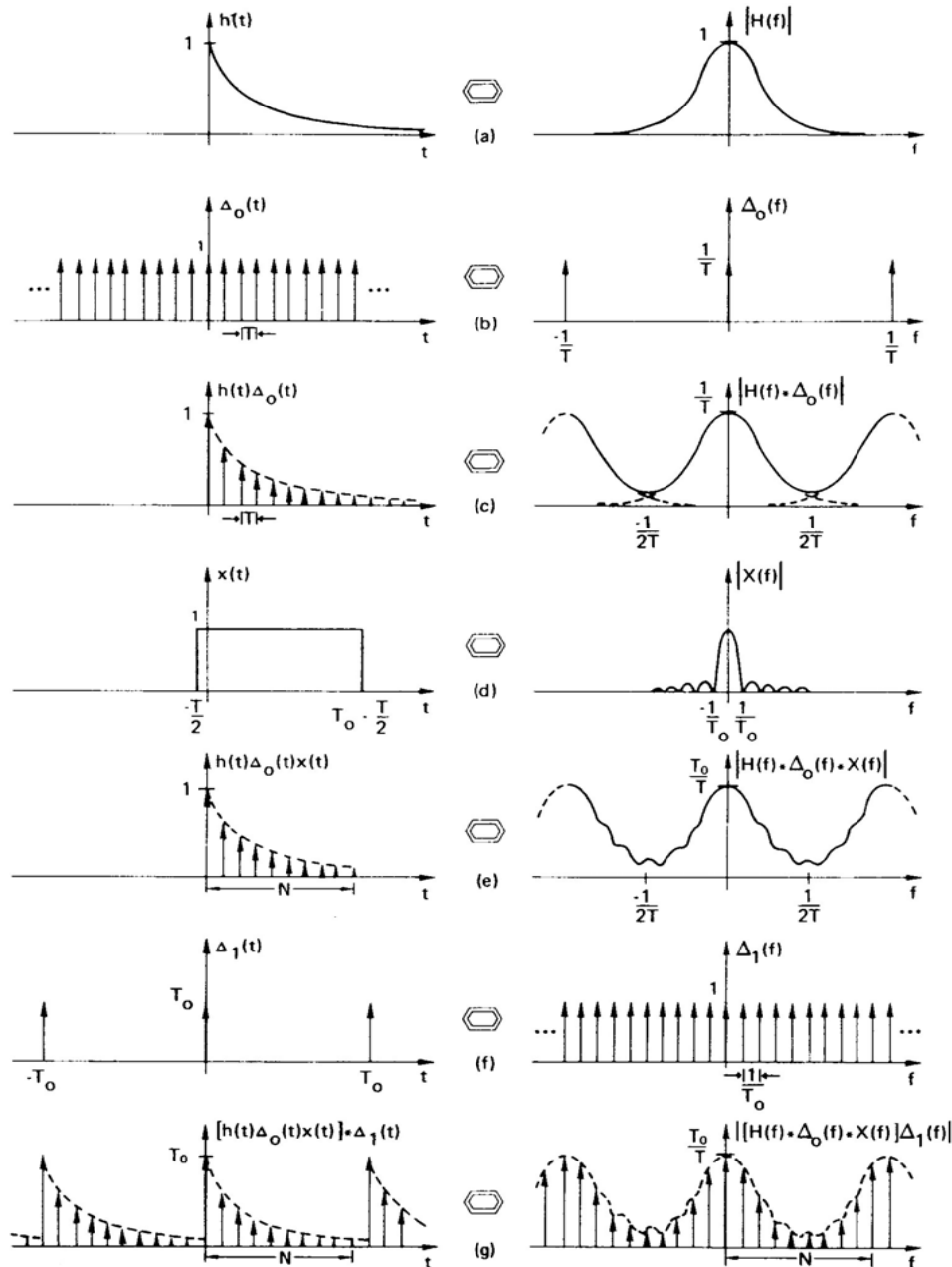
$x(t) = h(x) * g(t)$ is time limited with twice the support of $h(t)$ or $g(t)$, i.e., non – zero in the domain $-2T_0 \leq t \leq 2T_0$

f) Parseval's theorem :

$$\int_{-\infty}^{\infty} h^2(t)e^{-2\pi\sigma t} dt = \int_{-\infty}^{\infty} H(f)H(\sigma - f)df$$

with $\sigma = 0$ and for $h(t)$ real: $\int_{-\infty}^{\infty} h^2(t)dt = \int_{-\infty}^{\infty} |H(f)|^2 df$

From the Continuous to the Discrete Fourier Transform



aliasing

leakage

periodic

The Discrete Fourier Transform

$$H(m\Delta f) = \sum_{k=0}^{N-1} h(k\Delta t) e^{-i2\pi k\Delta t m\Delta f} \Delta t = \sum_{k=0}^{N-1} h(k\Delta t) e^{-i2\pi km/N} \Delta t$$

$$h(k\Delta t) = \sum_{m=0}^{N-1} H(m\Delta f) e^{i2\pi k\Delta t m\Delta f} \Delta f = \sum_{m=0}^{N-1} H(m\Delta f) e^{i2\pi km/N} \Delta f$$

$$T_o = \frac{1}{\Delta f} = N\Delta t, \quad F_o = \frac{1}{\Delta t} = N\Delta f, \quad |f_N| = \frac{F_o}{2} = \frac{1}{2\Delta t}$$

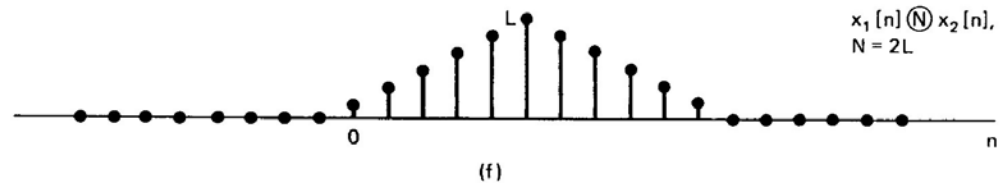
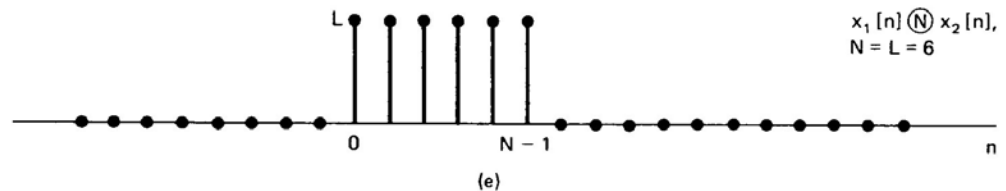
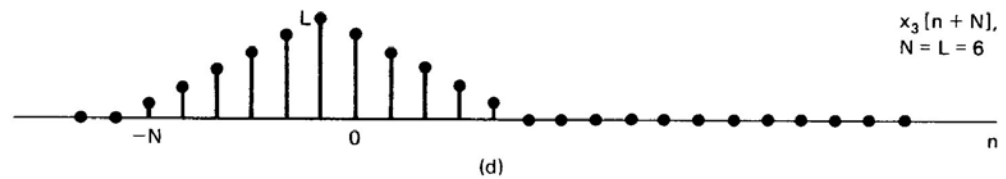
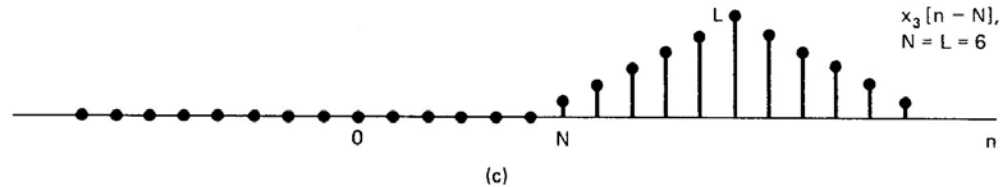
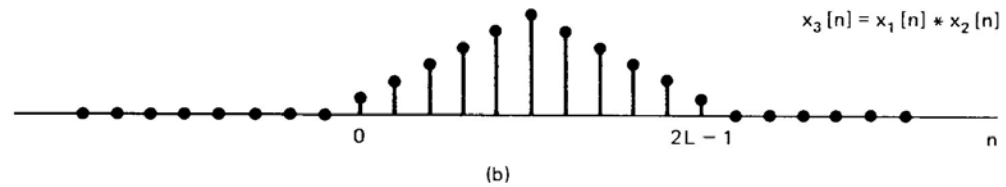
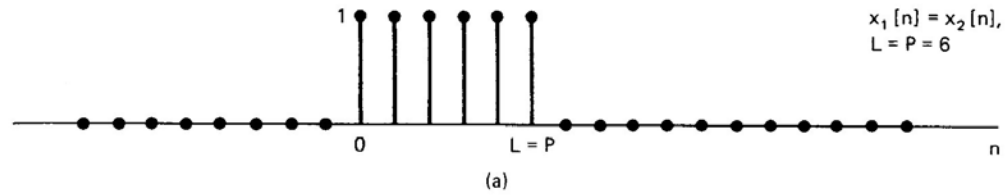
$$h(k\Delta t) \leftrightarrow H(m\Delta f) \quad \text{or} \quad h(t_k) \leftrightarrow H(f_m) \quad \text{or} \quad h(k) \leftrightarrow H(m)$$

Discrete and circular convolution and correlation

$$x(k) = \sum_{l=0}^{N-1} g(l)h(k-l)\Delta t = g(k) * h(k) \quad y(k) = \sum_{l=0}^{N-1} g(l)h(k+l)\Delta t = g(k) \otimes h(k)$$

$$x(k) = \mathbf{F}^{-1} \{ \mathbf{F} \{ g(k) \} \mathbf{F} \{ h(k) \} \} \quad y(k) = \mathbf{F}^{-1} \{ \mathbf{F} \{ g(k) \} [\mathbf{F} \{ h(k) \}]^* \}$$

Circular Convolution as Linear Convolution Plus Aliasing



CR, CV and PSD Functions

Definitions:

$$R_{gh}(t_k) = \mathbf{E}\{g(t_l)h(t_k + t_l)\} = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{l=0}^{N-1} g(t_l)h(t_k + t_l) = \lim_{T_o \rightarrow \infty} \frac{1}{T_o} g(t_k) \otimes h(t_k)$$

$$\begin{aligned} C_{gh}(t_k) &= \mathbf{E}\{[g(t_l) - \bar{g}][h(t_k + t_l) - \bar{h}]\} = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{l=0}^{N-1} [g(t_l) - \bar{g}][h(t_k + t_l) - \bar{h}] \\ &= \lim_{T_o \rightarrow \infty} \frac{1}{T_o} g(t_k) \otimes h(t_k) - \bar{g}\bar{h} = R_{gh}(t_k) - \bar{g}\bar{h} \end{aligned}$$

$$P_{gh}(f_m) = \mathbf{F}\{R_{gh}(t_k)\} = \lim_{T_o \rightarrow \infty} \frac{1}{T_o} G(f_m)H^*(f_m)$$

Computation by FFT:

$$\hat{P}_{gh}(f_m) = \frac{1}{vT_o} \sum_{\lambda=1}^v G_{\lambda}(f_m)H_{\lambda}^*(f_m)$$

$$\hat{R}_{gh}(t_k) = \mathbf{F}^{-1}\{\hat{P}_{gh}(f_m)\}$$

$$\hat{C}_{gh}(t_k) = \mathbf{F}^{-1}\{\hat{P}_{gh}(f_m) - \bar{g}\bar{h}\delta(f_m)\}$$

The DFT in Computers

Subroutines usually assume $\Delta t = 1$ and also ignore T_0 .

This requires rescaling as follows:

$$H(f_m) = T_0 H_c(m) = N \Delta t H_c(m)$$

$$x(t_k) = g(t_k) * h(t_k) = T_0 x_c(t_k) = T_0 F_c^{-1} \{G_c(m) H_c(m)\}$$

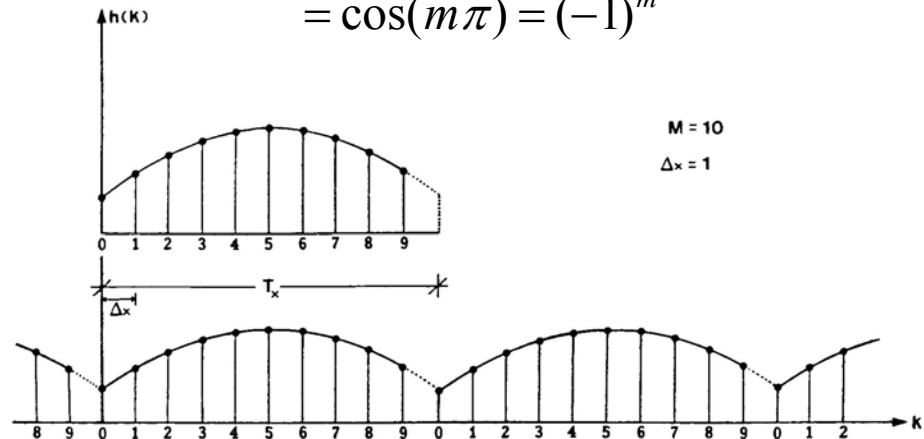
It also yields: $H_c(0) = \bar{h}$

Subroutines also assume the origin at the left of the record.

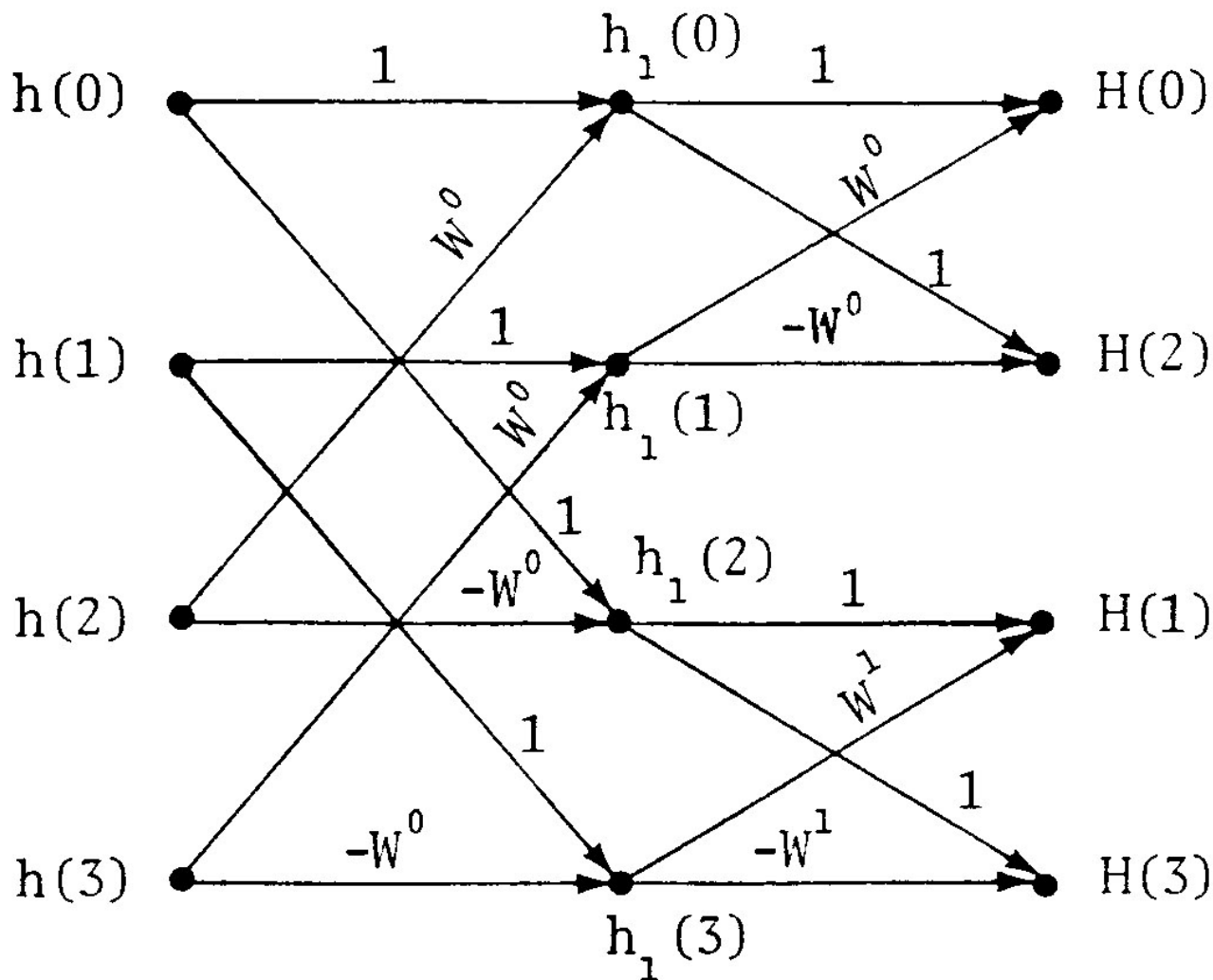
This requires changing the phase of the spectrum by $e^{-i2\pi m \Delta f T_0 / 2} = e^{-i\pi m}$

$$h(t_k - T_0 / 2) \leftrightarrow (-1)^m H(f_m) = \cos(m\pi) = (-1)^m$$

End point of a period
must be omitted
(assumed due to periodicity)



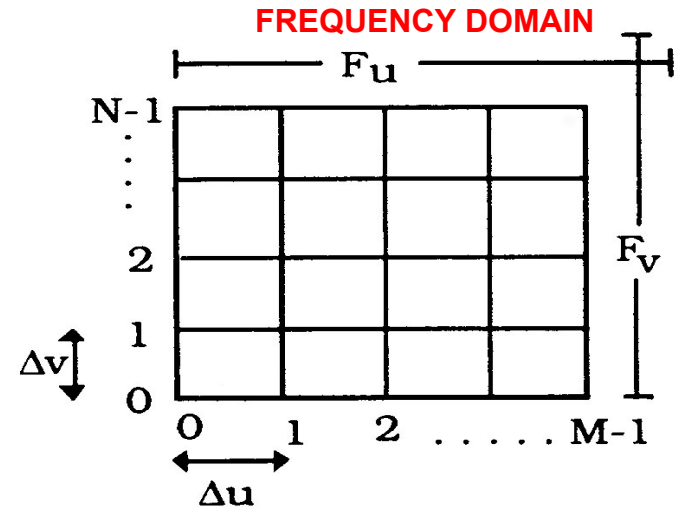
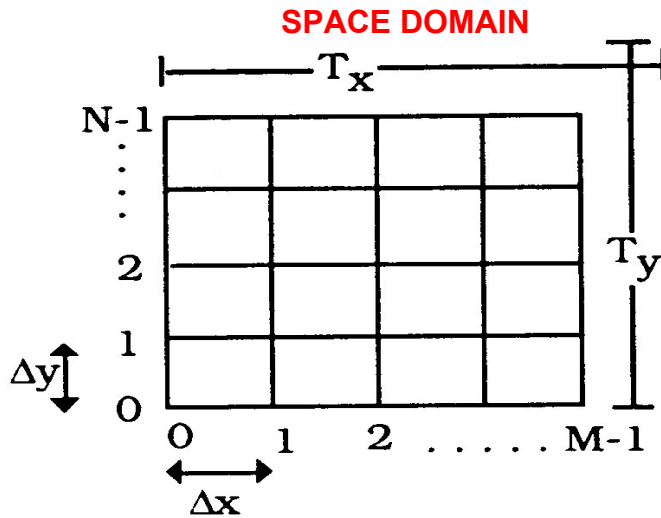
The FFT - Flow Graph of Operations for N=4



The Two-dimensional DFT

$$H(u_m, v_n) = \sum_{k=0}^{M-1} \sum_{l=0}^{N-1} h(x_k, y_l) e^{-i2\pi(mk/M + nl/N)} \Delta x \Delta y$$

$$h(x_k, y_l) = \sum_{m=0}^{M-1} \sum_{n=0}^{N-1} H(u_m, v_n) e^{i2\pi(mk/M + nl/N)} \Delta u \Delta v$$



$$\Delta u = \frac{1}{T_y} = \frac{1}{M\Delta x},$$

$$\Delta v = \frac{1}{T_x} = \frac{1}{N\Delta y}$$

$$\Delta x = \frac{1}{F_u} = \frac{1}{M\Delta u} = \frac{1}{2u_N},$$

$$\Delta y = \frac{1}{F_v} = \frac{1}{N\Delta v} = \frac{1}{2v_N}$$



Geoid Undulations by FFT

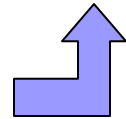
Geoid Undulations by FFT (1/9)

PLANAR APPROXIMATION OF STOKES'S INTEGRAL

$$N(x_P, y_P) = \frac{1}{2\pi\gamma} \iint_E \frac{\Delta g(x, y)}{\sqrt{(x_P - x)^2 + (y_P - y)^2}} dx dy = \frac{1}{\gamma} \Delta g(x_P, y_P) * l_N(x_P, y_P)$$

FFT: two direct
and one inverse
Fourier transform

$$l_N(x, y) = (2\pi)^{-1} (x^2 + y^2)^{-1/2}$$



$$N(x, y) = \frac{1}{\gamma} F^{-1} \{ F \{ \Delta g(x, y) \} F \{ l_N(x, y) \} \} = \frac{1}{\gamma} F^{-1} \{ \Delta G(u, v) L_N(u, v) \}$$

Geoid Undulations by FFT (2/9)

Point Gravity Anomalies as Input

$$N(x_k, y_l) = \frac{1}{\gamma} \sum_{i=0}^{M-1} \sum_{j=0}^{N-1} \Delta g(x_i, y_j) l_N(x_k - x_i, y_l - y_j) \Delta x \Delta y$$

FFT: two direct
and one inverse
Fourier transform

$$l_N(x_k - x_i, y_l - y_j) = \begin{cases} (2\pi)^{-1} [(x_k - x_i)^2 + (y_l - y_j)^2]^{-1/2}, & x_k \neq x_i \text{ or } y_l \neq y_j \\ 0, & x_k = x_i \text{ and } y_l = y_j \end{cases}$$

$$N(x_k, y_l) = \frac{1}{2\pi\gamma} \mathbf{F}^{-1} \{ \Delta G(u_m, v_n) L_N(u_m, v_n) \}$$

$$L_N(u_m, v_n) = \mathbf{F} \{ l_N(x_k, y_l) \} = \sum_{k=0}^{M-1} \sum_{l=0}^{N-1} l_N(x_k, y_l) e^{-j2\pi(mk/M + nl/N)} \Delta x \Delta y$$

$$\Delta G(u_m, v_n) = \mathbf{F} \{ \Delta g(x_k, y_l) \} = \sum_{k=0}^{M-1} \sum_{l=0}^{N-1} \Delta g(x_k, y_l) e^{-j2\pi(mk/M + nl/N)} \Delta x \Delta y$$

Geoid Undulations by FFT (3/9)

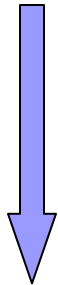
Mean Gravity Anomalies as Input

$$N(x_k, y_l) = \frac{1}{2\pi\gamma} \sum_{i=0}^{M-1} \sum_{j=0}^{N-1} \Delta g(x_i, y_j) \bar{l}_N(x_k - x_i, y_l - y_j)$$



$$\bar{l}_N(x_k, y_l) = \int_{x_k - \Delta x/2}^{x_k + \Delta x/2} \int_{y_l - \Delta y/2}^{y_l + \Delta y/2} \frac{1}{\sqrt{x^2 + y^2}} dx dy$$

$$= x \ln(y + \sqrt{x^2 + y^2}) + y \ln(x + \sqrt{x^2 + y^2}) \Big|_{x_k - \Delta x/2}^{x_k + \Delta x/2} \Big|_{y_l - \Delta y/2}^{y_l + \Delta y/2}$$



FFT: two direct
and one inverse
Fourier transform

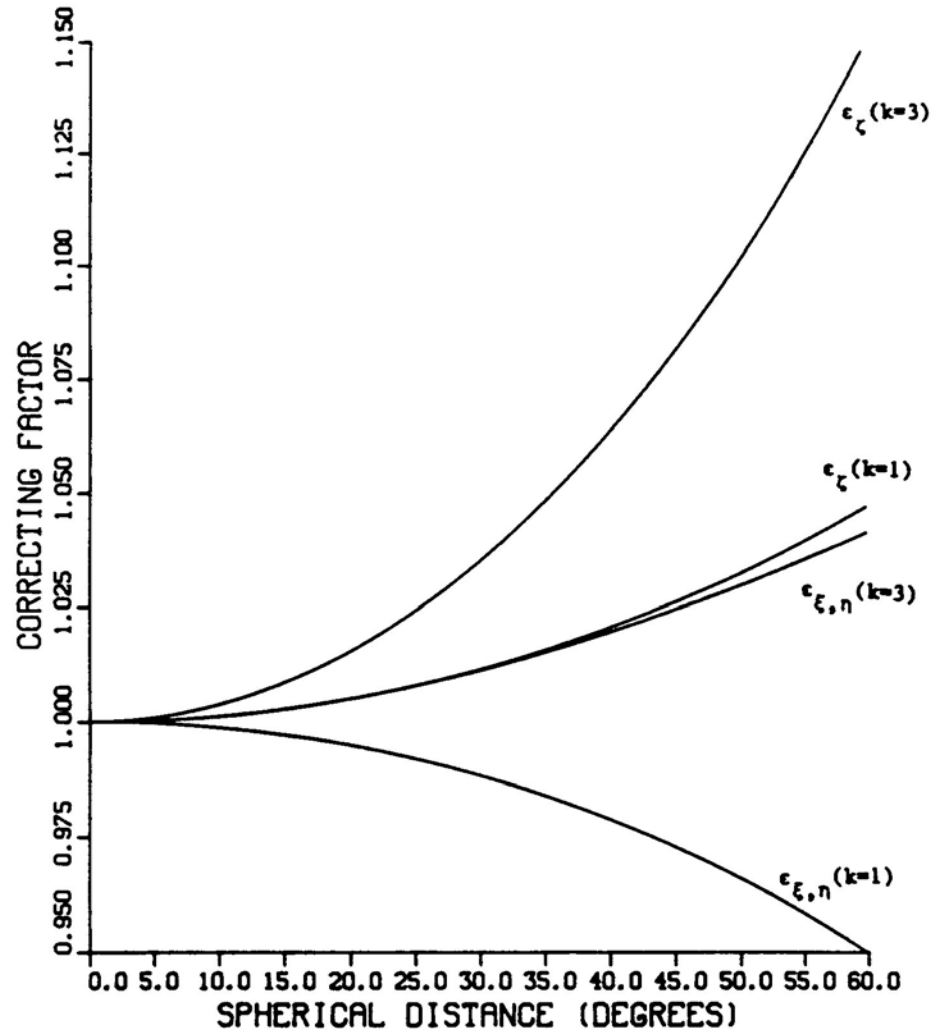
$$N(x_k, y_l) = \frac{1}{2\pi\gamma} \mathbf{F}^{-1} \{ \mathbf{F} \{ \Delta g(x_k, y_l) \} \mathbf{F} \{ \bar{l}_N(x_k, y_l) \} \} = \frac{1}{2\pi\gamma} \mathbf{F}^{-1} \{ \Delta G(u_m, v_n) \bar{L}_N(u_m, v_n) \}$$

Geoid Undulations by FFT (4/9)

Effects of Planar Approximation - Spherical Corrections

Factors for correcting planar ξ , η , N (or T or ζ) for the Earth's curvature

To avoid long-wavelength errors, the area of local data should not extend to more than several hundreds of kilometers in each direction.



Geoid Undulations by FFT (5/9)

Spherical form of Stokes's Integral

$$N(\varphi_p, \lambda_p) = \frac{R}{4\pi\gamma} \iint_E \Delta g(\varphi, \lambda) S(\varphi_p, \lambda_p, \varphi, \lambda) \cos \varphi \, d\varphi d\lambda$$

$$N(\varphi_l, \lambda_k) = \frac{R}{4\pi\gamma} \sum_{j=0}^{N-1} \sum_{i=0}^{M-1} \Delta g(\varphi_j, \lambda_i) \cos \varphi_j S(\varphi_l, \lambda_k, \varphi_j, \lambda_i) \Delta\varphi \Delta\lambda$$

With different approximations of Stokes's kernel function on the sphere, geoid undulations can be evaluated at all gridded points simultaneously by means of either the one-dimensional or the two-dimensional fast Fourier transform

Geoid Undulations by FFT (6/9)

Approximated Spherical Kernel

$$\cos \phi_P \cos \phi \xrightarrow{\text{approximation}} \cos^2 \bar{\phi} - \sin^2 (\phi_P - \phi) / 2$$

$$\sin^2 \frac{\psi}{2} = \sin^2 \frac{\varphi_P - \varphi}{2} + \sin^2 \frac{\lambda_P - \lambda}{2} \cos \varphi_P \cos \varphi$$

$$\begin{aligned} \downarrow \quad \sin^2 \frac{\psi}{2} &\approx \sin^2 \frac{\varphi_P - \varphi}{2} + \sin^2 \frac{\lambda_P - \lambda}{2} \cos^2 \bar{\varphi} \\ &\approx \sin^2 \frac{\varphi_P - \varphi}{2} + \sin^2 \frac{\lambda_P - \lambda}{2} (\cos^2 \bar{\varphi} - \sin^2 \frac{\varphi_P - \varphi}{2}) \end{aligned}$$

$$N(\varphi_l, \lambda_k) = \frac{R}{4\pi\gamma} \sum_{j=0}^{N-1} \sum_{i=0}^{M-1} \Delta g(\varphi_j, \lambda_i) \cos \varphi_j S(\varphi_l - \varphi_j, \lambda_k - \lambda_i, \bar{\varphi}) \Delta \varphi \Delta \lambda$$

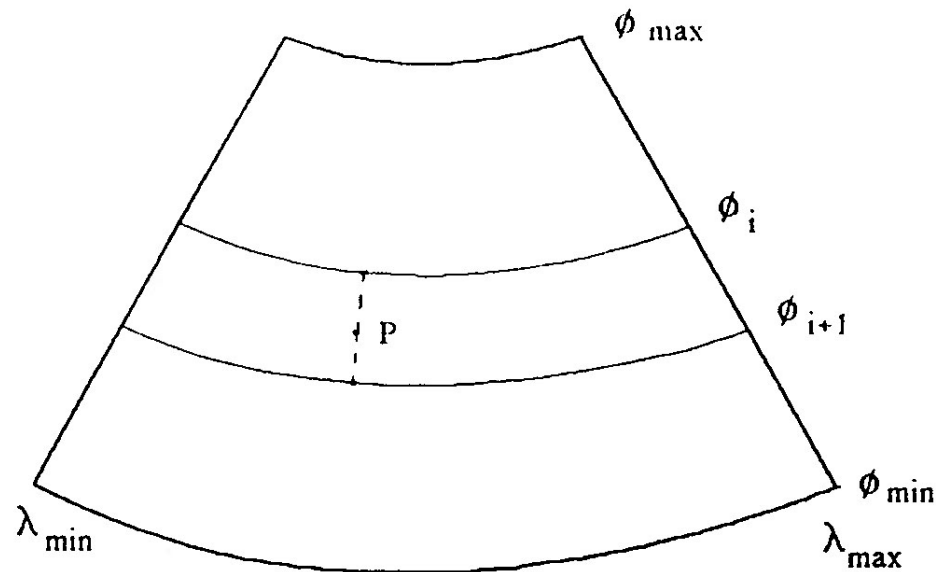
$$= \frac{R}{4\pi\gamma} [\Delta g(\varphi_l, \lambda_k) \cos \varphi_l] * S(\varphi_l, \lambda_k, \bar{\varphi}).$$

$$\downarrow \quad N(\varphi_l, \lambda_k) = \frac{R}{4\pi\gamma} \mathbf{F}^{-1} \{ \mathbf{F} \{ \Delta g(\varphi_l, \lambda_k) \cos \varphi_l \} \mathbf{F} \{ S(\varphi_l, \lambda_k, \bar{\varphi}) \} \}$$

Geoid Undulations by FFT (7/9)

Latitude bands used in the multi-band spherical FFT approach

$$\begin{aligned}\sin^2 \frac{\psi}{2} &\approx \sin^2 \frac{\varphi_p - \varphi}{2} + \sin^2 \frac{\lambda_p - \lambda}{2} \cos \bar{\varphi}_i \cos[\bar{\varphi}_i - (\bar{\varphi}_i - \varphi)] \\ &\approx \sin^2 \frac{\varphi_p - \varphi}{2} + \sin^2 \frac{\lambda_p - \lambda}{2} [\cos^2 \bar{\varphi}_i \cos(\bar{\varphi}_i - \varphi) + \cos \bar{\varphi}_i \sin \bar{\varphi}_i \sin(\bar{\varphi}_i - \varphi)]\end{aligned}$$

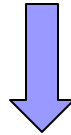


Geoid Undulations by FFT (8/9)

Rigorous Spherical Kernel

$$N(\varphi_l, \lambda_k) = \frac{R}{4\pi\gamma} \sum_{j=0}^{N-1} \left[\sum_{i=0}^{M-1} \Delta g(\varphi_j, \lambda_i) \cos \varphi_j S(\varphi_l, \varphi_j, \lambda_k - \lambda_i) \Delta \lambda \right] \Delta \varphi, \quad \varphi_l = \varphi_1, \varphi_2, \dots, \varphi_N$$

Addition Theorem of DFT



$$N(\varphi_l, \lambda_k) = \frac{R}{4\pi\gamma} \mathbf{F}_1^{-1} \left\{ \sum_{j=0}^{N-1} \mathbf{F}_1 \{ \Delta g(\varphi_j, \lambda_k) \cos \varphi_j \} \mathbf{F}_1 \{ S(\varphi_l, \varphi_j, \lambda_k) \} \right\}, \quad \varphi_l = \varphi_1, \varphi_2, \dots, \varphi_N$$

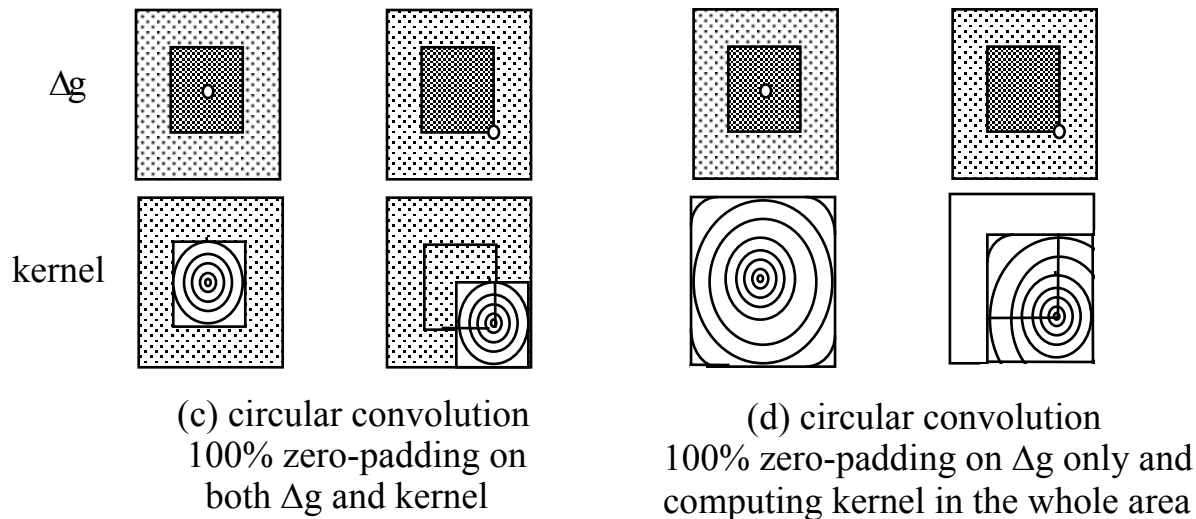
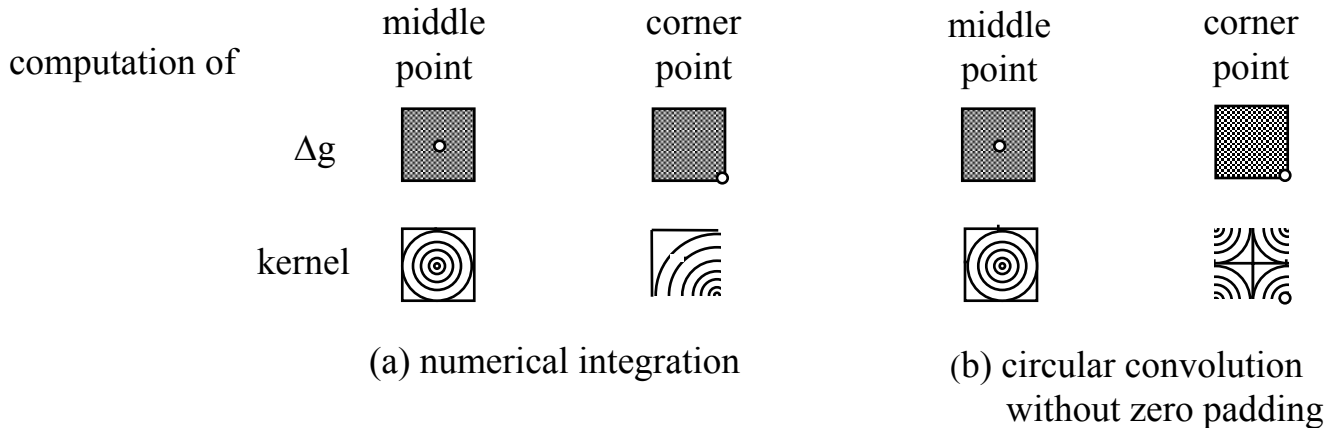
The advantage of the 1D spherical FFT approach: it gives exactly the same results as those obtained by direct numerical integration. It only needs to deal with one one-dimensional complex array each time, resulting in a considerable saving in computer memory as compared to the 2D FFT technique discussed before.

Geoid Undulations by FFT (9/9)

Computational procedure:

- Subtract effect of GM from Δg (long wavelength)
- Subtract effect of terrain from Δg (short wavelength)
- Use the reduced Δg in the FFT formulas
- Add to the results (reduced co-geoid) the GM effect
- Add to the results (reduced co-geoid) the indirect terrain effects

Edge Effects and Circular Convolution - Zero Padding





Optimal Spectral Geoid Determination

Error propagation (1/2)

FFT method can use heterogeneous data, provided that they are given on a grid, and can produce error estimates, provided the PSDs (the Fourier transform of the covariance functions) of the data and their noise are known and stationary

$$(\Delta g + n) * s + \varepsilon = N, \quad s = \frac{l_N}{\gamma}$$

$$F\{N\} = (F\{\Delta g\} + F\{n\})F\{s\} + F\{e\}$$

Multiplying by the complex conjugate of $F\{N\}$ first and then by the complex conjugate of $F\{\Delta g\}$, we get :

$$P_{NN} = P_{ee} + S(P_{\Delta g \Delta g} + P_{nn})S^* = P_{ee} + |S|^2 (P_{\Delta g \Delta g} + P_{nn})$$

$$P_{N \Delta g} = S(P_{\Delta g \Delta g} + P_{nn})$$

No correlation between signal and noise and between input and output noise

S is the spectrum of s , and $P_{\Delta g \Delta g}$ is the PSD of the gravity anomalies

Error Propagation (2/2)

$$F\{N\} = F\{\Delta g\}F\{s\} = P_{N\Delta g} (P_{\Delta g\Delta g} + P_{nn})^{-1} F\{\Delta g\}$$

spectral form

$$S = P_{N\Delta g} (P_{\Delta g\Delta g} + P_{nn})^{-1} = S_0 \left(1 + \frac{P_{nn}}{P_{\Delta g\Delta g}}\right)^{-1}, \quad S_0 = \frac{P_{N\Delta g}}{P_{\Delta g\Delta g}}$$



$$\hat{N} = C_{N\Delta g} (C_{\Delta g\Delta g} + C_{nn})^{-1} \Delta g$$

collocation form

$$P_{ee} = P_{NN} - P_{N\Delta g} (P_{\Delta g\Delta g} + P_{nn})^{-1} P_{\Delta gN} = |S_0|^2 P_{\Delta g\Delta g} \left[1 - \left(1 + \frac{P_{nn}}{P_{\Delta g\Delta g}}\right)^{-1}\right]$$

spectral form



$$C_{ee} = C_{NN} - C_{N\Delta g} (C_{\Delta g\Delta g} + C_{nn})^{-1} C_{N\Delta g}^T$$

collocation form



Other Applications of FFT

Application 1: Terrain Corrections by FFT (1/2)

Conventional Computation of TC

- Single point computation
- Numerical integration: summation of contributions of compartments (prisms)
- Time consuming: $t \sim N^2$

FFT Computation of TC

- Convolution integral
- Homogeneous TC coverage for BVPs
- Height files on regular grid
- Need for faster methods → **FFT approach ideal**
- Reduced computation time: $t \sim N \log N$
- Handling of large amounts of gridded data
- Spectral analysis; covariance functions

DATA: gridded h (and ρ)

OBJECTIVE: Rigorous and fast evaluation of TC integral

Terrain Corrections by FFT(2/2)

$$\begin{aligned}
 c(x_P, y_P) &= \frac{1}{2} k\rho \iint_E \frac{h^2(x, y) - h^2(x_P, y_P)}{[(x_P - x)^2 + (y_P - y)^2]^{3/2}} dx dy \\
 &\quad - h(x_P, y_P) k\rho \iint_E \frac{h(x, y) - h(x_P, y_P)}{[(x_P - x)^2 + (y_P - y)^2]^{3/2}} dx dy \\
 &= \frac{1}{2} k\rho \{ h^2(x_P, y_P) * l_c(x_P, y_P) - h^2(x_P, y_P) [o(x_P, y_P) * l_c(x_P, y_P)] \\
 &\quad - 2h(x_P, y_P) [h(x_P, y_P) * l_c(x_P, y_P) - h(x_P, y_P) [o(x_P, y_P) * l_c(x_P, y_P)]] \}
 \end{aligned}$$

where $l_c(x, y) = (x^2 + y^2)^{-3/2}$ and $o(x, y) = 1$

PROCEDURE

- Transform $h, h_2=h^2, o, l_c$ to H, H_2, O, L_c (direct FFT) and form $H L_c, H_2 L_c, O L_c$
- Transform $H L_c, H_2 L_c, O L_c$ to $h * l_c, h_2 * l_c, o * l_c$ (inverse FFT)
- Multiply and add/subtract terms as needed

$$\begin{aligned}
 c(x, y) &= \frac{1}{2} k\rho \{ F^{-1} \{ H_2(u, v) L_c(u, v) \} - h^2(x, y) F^{-1} \{ O(u, v) L_c(u, v) \} \\
 &\quad - 2h(x, y) [F^{-1} \{ H(u, v) L_c(u, v) \} - h(x, y) F^{-1} \{ O(u, v) L_c(u, v) \}] \}
 \end{aligned}$$

Application 2:

Stokes and Vening Meinesz on the plane (1/2)

$$N(x_p, y_p) = \frac{1}{2\pi\gamma} \iint_E \Delta g(x, y) \frac{1}{[(x_p - x)^2 + (y_p - y)^2]^{1/2}} = \frac{1}{2\pi\gamma} \Delta g(x_p, y_p) * l_N(x_p, y_p)$$

$$l_N(x, y) = (x^2 + y^2)^{-1/2}$$

$$\begin{aligned} \begin{Bmatrix} \xi(x_p, y_p) \\ \eta(x_p, y_p) \end{Bmatrix} &= \begin{Bmatrix} -\partial N(x_p, y_p) / \partial y_p \\ -\partial N(x_p, y_p) / \partial x_p \end{Bmatrix} = -\frac{1}{2\pi\gamma} \begin{Bmatrix} \Delta g(x_p, y_p) * \partial l_N(x_p, y_p) / \partial y_p \\ \Delta g(x_p, y_p) * \partial l_N(x_p, y_p) / \partial x_p \end{Bmatrix} \\ &= -\frac{1}{2\pi\gamma} \Delta g(x_p, y_p) * \begin{Bmatrix} l_\xi(x_p, y_p) \\ l_\eta(x_p, y_p) \end{Bmatrix} \end{aligned}$$

$$\begin{Bmatrix} l_\xi(x, y) \\ l_\eta(x, y) \end{Bmatrix} = -\begin{Bmatrix} \partial l_N(x, y) / \partial y \\ \partial l_N(x, y) / \partial x \end{Bmatrix} = (x^2 + y^2)^{-3/2} \begin{Bmatrix} y \\ x \end{Bmatrix}$$

$$\begin{Bmatrix} \xi(x_p, y_p) \\ \eta(x_p, y_p) \end{Bmatrix} = \frac{1}{2\pi\gamma} \iint_E \Delta g(x, y) \frac{1}{[(x_p - x)^2 + (y_p - y)^2]^{3/2}} \begin{Bmatrix} y_p - y \\ x_p - x \end{Bmatrix} dx dy$$

Stokes and Vening Meinesz on the plane (2/2)

Since $L_N(u, v) = \mathbf{F}\{l_N(x, y)\} = \mathbf{F}\{(x^2 + y^2)^{-1/2}\} = (u^2 + v^2)^{1/2}$

$$\begin{cases} l_\xi(x, y) \\ l_\eta(x, y) \end{cases} = - \begin{cases} \partial l_N(x, y) / \partial y \\ \partial l_N(x, y) / \partial x \end{cases}$$

then

$$\mathbf{F} \begin{cases} \xi(x, y) \\ \eta(x, y) \end{cases} = -\frac{1}{2\pi\gamma} \Delta G(u, v) \begin{cases} 2\pi i u \\ 2\pi i v \end{cases} L_N(u, v)$$

$$N(x, y) = \frac{1}{2\pi\gamma} \mathbf{F}^{-1} \left\{ \Delta G(u, v) \frac{1}{(u^2 + v^2)^{1/2}} \right\}$$

**High-frequency attenuation
(integration)**

$$\begin{cases} \xi(x, y) \\ \eta(x, y) \end{cases} = -\frac{1}{\gamma} \mathbf{F}^{-1} \begin{cases} \Delta G(u, v) \frac{iv}{(u^2 + v^2)^{1/2}} \\ \Delta G(u, v) \frac{i u}{(u^2 + v^2)^{1/2}} \end{cases}$$

**High-frequency amplification
(differentiation)**

Application 3: Analytical Continuation

Upward continuation from $h=0$ to $h=z_0$

$$\begin{aligned}\Delta g(x_P, y_P, z_0) &= \frac{1}{2\pi} \iint_E \Delta g(x, y, 0) \frac{z_0}{[(x_P - x)^2 + (y_P - y)^2 + z_0^2]^{3/2}} dx dy \\ &= \Delta g(x_P, y_P, 0) * l_u(x_P, y_P, z_0), \quad l_u(x, y, z_0) = \frac{z_0}{2\pi[(x^2 + y^2 + z_0^2)^{3/2}] \\ &= \mathbf{F}^{-1} \{ \mathbf{F} \{ \Delta g(x_P, y_P, 0) \} \mathbf{F} \{ l_u(x_P, y_P, z_0) \} \}\end{aligned}$$

Analytical spectrum of l_u : $\mathbf{F} \{ l_u(x_P, y_P, z_0) \} = L_u(u, v, z_0) = e^{-2\pi z_0(u^2 + v^2)^{1/2}}$

High-frequency attenuation

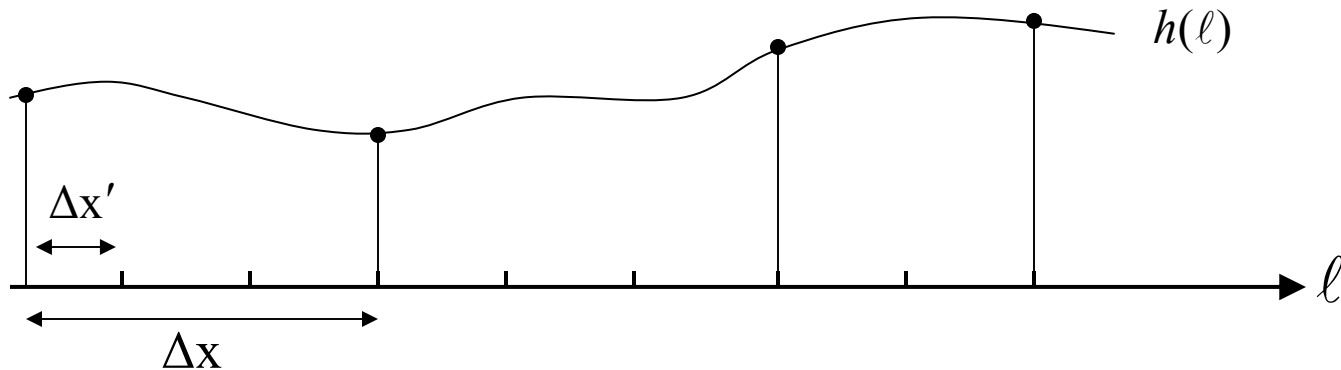
Downward continuation from $h=z_0$ to $h=0$

$$\Delta g(x_P, y_P, 0) = \mathbf{F}^{-1} \left\{ \frac{\mathbf{F} \{ \Delta g(x_P, y_P, z_0) \}}{\mathbf{F} \{ l_u(x_P, y_P, z_0) \}} \right\} = \mathbf{F}^{-1} \{ \mathbf{F} \{ \Delta g(x_P, y_P, z_0) \} \mathbf{F} \{ l_d(x_P, y_P, z_0) \} \}$$

Analytical spectrum of l_d : $\mathbf{F} \{ l_d(x_P, y_P, z_0) \} = 1/L_u(u, v, z_0) = e^{2\pi z_0(u^2 + v^2)^{1/2}}$

High-frequency amplification

Application 4: Interpolation by FFT



- Want to interpolate with spacing $\Delta x' = \Delta x / L$
- Zeros are filled at $L-1$ points between the initial pairs of sampled values

$$g(\ell) = \begin{cases} h(\ell/L), & \ell = 0 \leq \ell \leq 2L \\ 0, & \text{elsewhere} \end{cases} \quad G(m) = H(mL) \quad \text{includes } m > \pm \frac{1}{L}$$

- Filter out higher frequencies, so that

$$-\frac{1}{L} \leq m \leq \frac{1}{L} \quad G_1(m) = \begin{cases} c \cdot H(mL), & -\frac{1}{L} \leq m \leq \frac{1}{L} \\ 0, & \text{elsewhere} \end{cases}$$

- Match initial amplitudes

$$g_1(0) = \frac{c}{L} h(0) \quad \rightarrow \quad c = L \quad \rightarrow \quad g_1(\ell) = F^{-1}\{G_1(m)\}$$



Concluding Remarks

Concluding Remarks

- Spectral methods can efficiently handle large amounts of gridded data and give results on all grid points simultaneously → **indispensable for geoid computations**
- Problems that affect the accuracy of the results: aliasing, leakage, singularity of the kernel functions at the origin, proper handling of mean and point data → **common to all methods using the same data**
- Problems unique to spectral methods:
 - Phase shifting
 - Edge effects and circular convolution
 - Planar approximation
- Drawbacks of FFT-based spectral techniques
 - Gridded data ONLY as input
 - Computer memory
 - Fast error propagation possible only with stationary noise



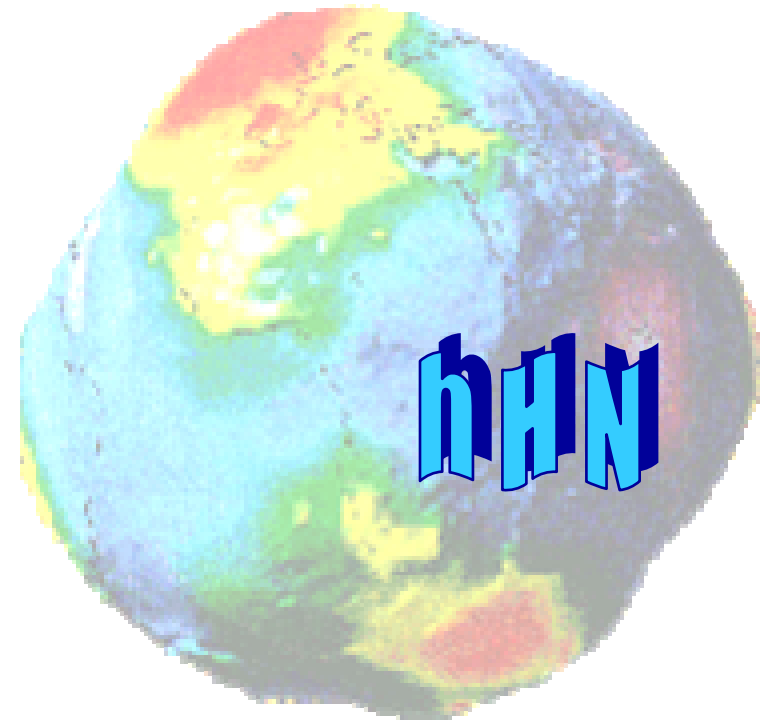
Matching the Gravimetric Geoid to the GPS-Levelling Undulations

Georgia Fotopoulos
gfotopou@ucalgary.ca

Department of Geomatics Engineering
University of Calgary

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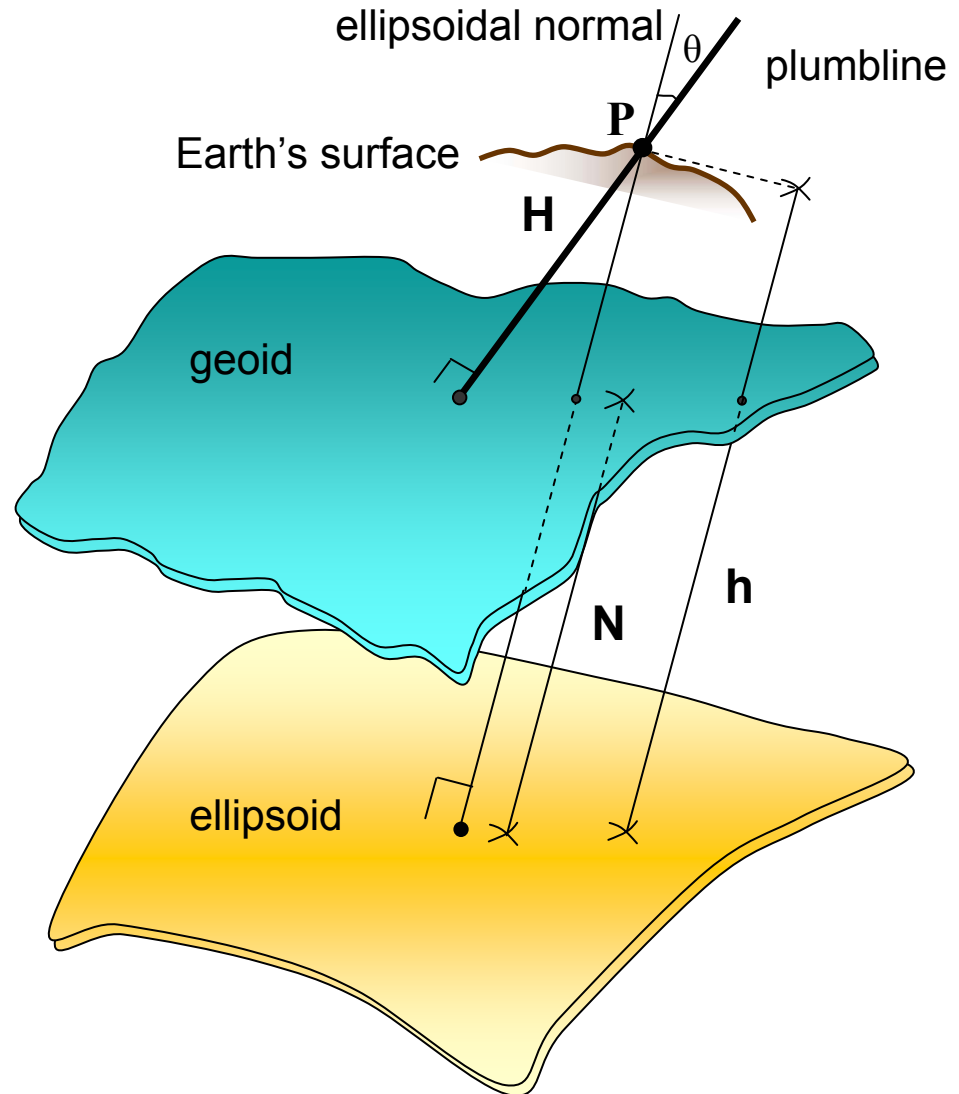
- Introduction to problem
- Why combine h , H and N ?
- Semi-automated parametric model testing procedure
 - classical empirical approach
 - cross-validation
 - measures of goodness of fit
 - testing parameter significance
- Examples
- Summary



Introduction

- Traditional means for establishing vertical control (**H**): spirit-levelling
 - ❑ costly
 - ❑ labourious
 - ❑ inefficient, difficult in remote areas, mountainous terrain, over large regions
- With advent of satellite-based global positioning systems (GPS) 3D positioning has been revolutionized

$$h - H - N = 0$$



Why combine h , H and N ?

- modernize regional vertical datums
- unify/connect national regional datums between neighbouring countries
- transform between different types of height data (GPS-levelling)
- refine and test existing gravimetric geoid models
- better understanding of data error sources
 - calibrate geoid error model
 - assess noise in GPS heights, test a-priori error measures
 - evaluate levelling precision, test a-priori error values
- Other applications: sea level change monitoring, post-glacial rebound studies, etc.

Introduction (continued)

Factors that cause discrepancies when combining heterogeneous heights:

- ❑ random errors in the derived heights h , H , and N
- ❑ datum inconsistencies inherent among the height types
- ❑ systematic effects and distortions (long-wavelength geoid errors, poorly modelled GPS errors and over-constrained levelling network adjustments)
- ❑ assumptions/theoretical approximations made in processing observed data (neglecting sea surface topography or river discharge corrections at tide gauges)
- ❑ approximate or inexact normal/orthometric height corrections
- ❑ instability of reference station monuments over time (geodynamic effects, land uplift/subsidence)

Problem Formulation

Standard practice: Use of a corrector surface to model the datum discrepancies and systematic effects when combining GPS, geoid and orthometric heights

Theory: $h_i - H_i - N_i = 0 \quad \rightarrow \quad N_i^{GPS/levelling} = N_i$

Practice: $h_i - H_i - N_i = l_i \quad \rightarrow \quad N_i^{GPS/levelling} \neq N_i$

Model: $l_i = h_i - H_i - N_i = \mathbf{a}_i^T \mathbf{x} + v_i$

parametric model

residuals

GNSS-Levelling

- Development of corrector surface models to be used with GPS and gravimetric geoid models for GPS-Levelling

$$H_p = h_p - N_p - \mathbf{a}_p^T \hat{\mathbf{x}}$$

↑
orthometric height at new point

known height data

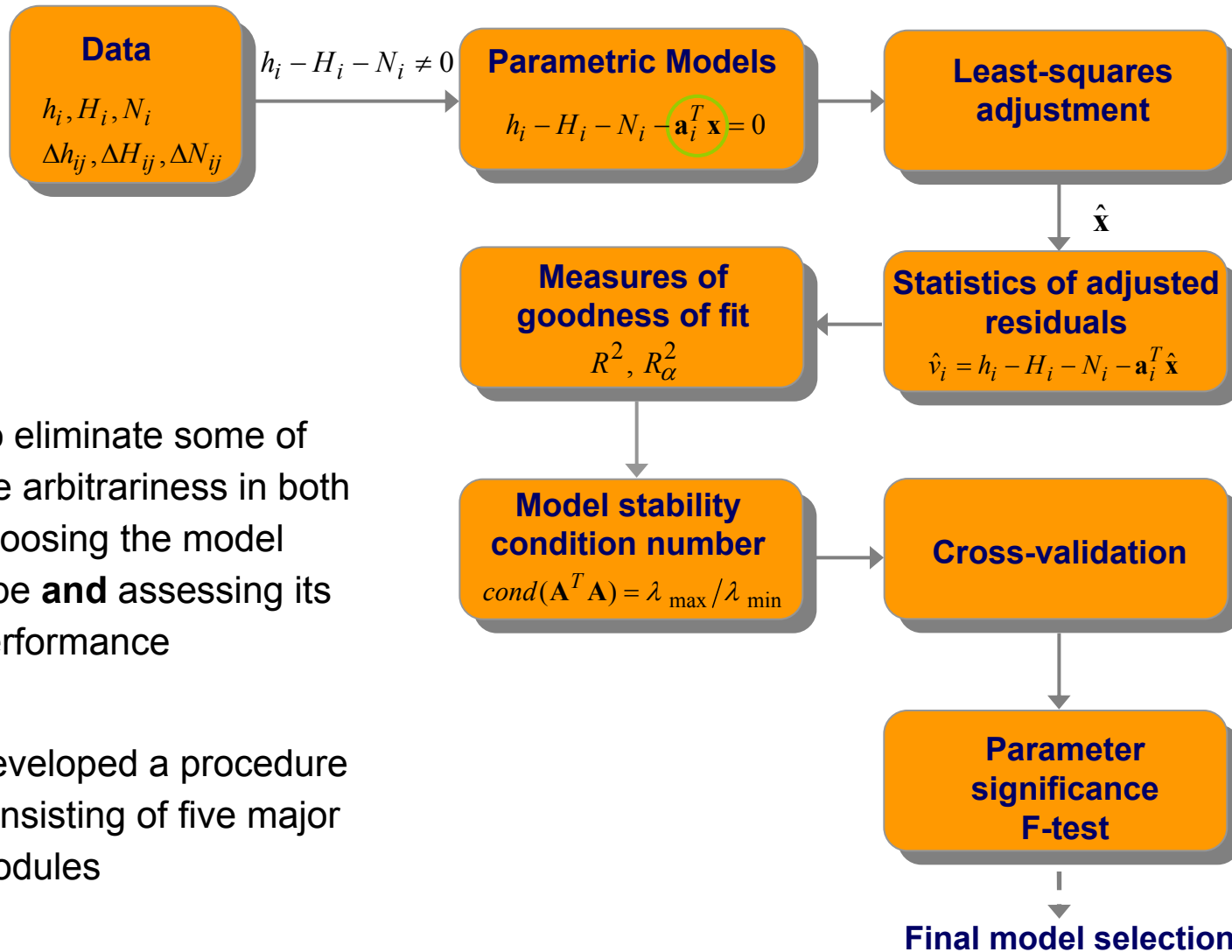
corrector surface

Data

GPS: $h_i, \Delta h_{ij}$ Orthometric heights: $H_i, \Delta H_{ij}$ Geoid model: $N_i, \Delta N_{ij}$

Prediction surface → aim is to derive a surface from data which is to be applied to new data

Semi-automated Parametric Model Testing Procedure



- To eliminate some of the arbitrariness in both choosing the model type **and** assessing its performance
- Developed a procedure consisting of five major modules

Parametric Surface Model Selection

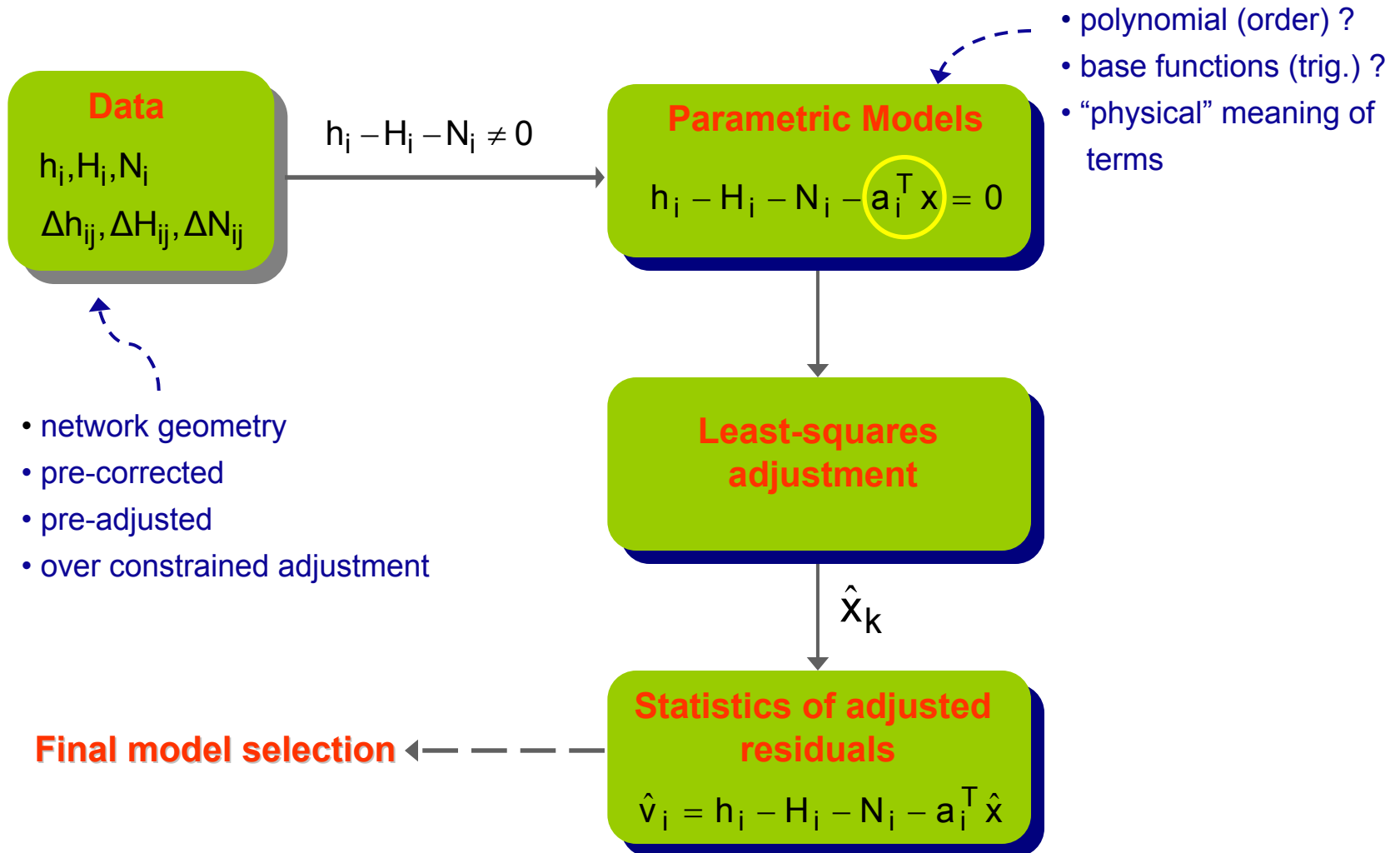
Parametric Models

$$h_i - H_i - N_i - \mathbf{a}_i^T \mathbf{x} = 0$$

- Selection of analytical model suffers from a degree of arbitrariness (*Why?*)
 - type of model (i.e. polynomial)
 - type of base functions (i.e. trigonometric)
 - number of coefficients
- Need statistical tools to
 - assess choices made
 - compare different models
- Factors for model selection/analysis may vary if
 - nested models
 - orthogonal vs. non-orthogonal models

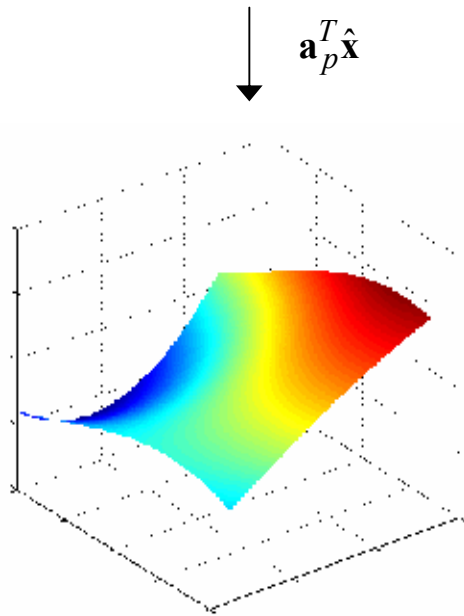
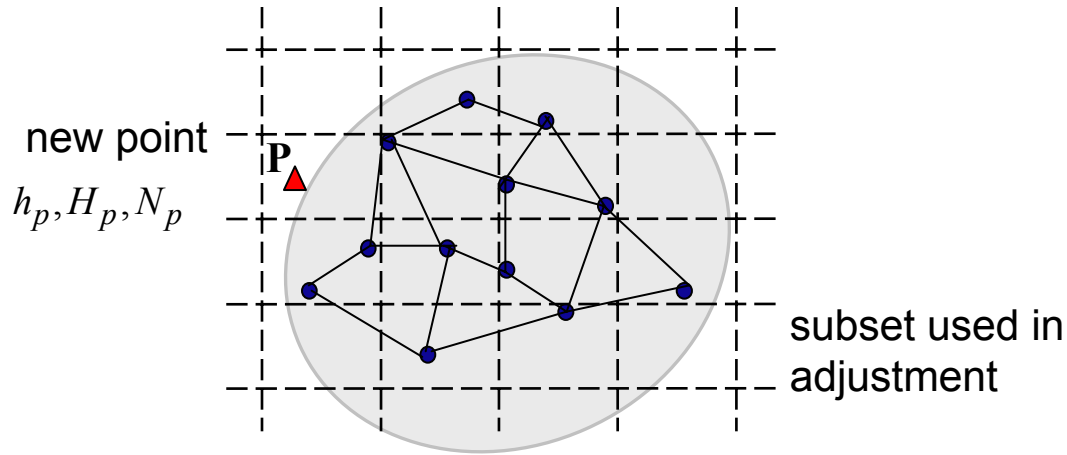
No straightforward answer, data dependent (geometry)

Classic Empirical Approach



Cross Validation

Cross-validation
(empirical approach)



$$\Delta \hat{v}_p = h_p - H_p - N_p - \mathbf{a}_p^T \hat{\mathbf{x}}$$

Repeat for each point and compute:

$$\frac{1}{n} \sum_{i=1}^n \sqrt{\mu_i^2 + \sigma_i^2}$$

Measures of Goodness of Fit

Statistics of adjusted residuals

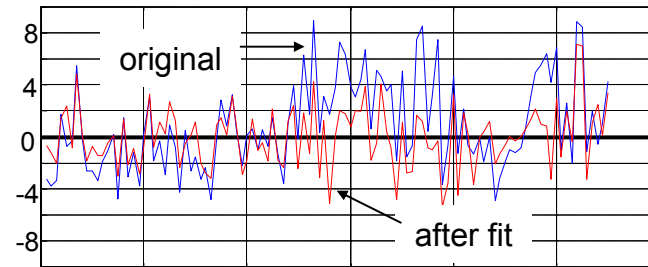
$$\hat{v}_i = h_i - H_i - N_i - a_i^T \hat{x}$$

Coefficient of determination

$$R^2$$

Adjusted coefficient of determination

$$\bar{R}^2$$



$$R^2 = 1 - \frac{\sum_{i=1}^n (l_i - \hat{v}_i)^2}{\sum_{i=1}^n (l_i - \bar{l}_i)^2}$$

$$l_i = h_i - H_i - N_i$$

n ... # of observations

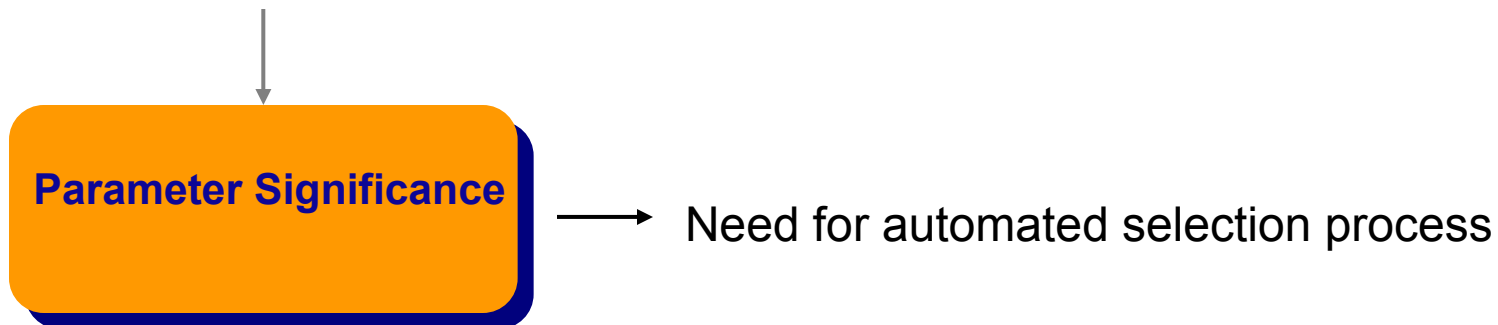
$$\bar{R}^2 = 1 - \frac{\left[\sum_{i=1}^n (l_i - \hat{v}_i)^2 \right] / (n-m)}{\left[\sum_{i=1}^n (l_i - \bar{l}_i)^2 \right] / (n-1)}$$

m ... # of parameters

Testing Parameter Significance

Reasons for reducing the number of model parameters

- Simplicity, computational efficiency
- Over-parameterization (i.e. high-degree trend models)
 - unrealistic extrema in data voids where control points are missing
- Unnecessary terms may bias other parameters in model
 - hinders capability to assess model performance



Stepwise Procedures

Backward Elimination Procedure

- Start with highest order model
- Eliminate less-significant terms one-by-one (or several at once)
- Criteria for determining parameter deletion
 - Partial F-test
 - Level of significance, α
 - **Problem:** correlation between parameters



nested
models
only

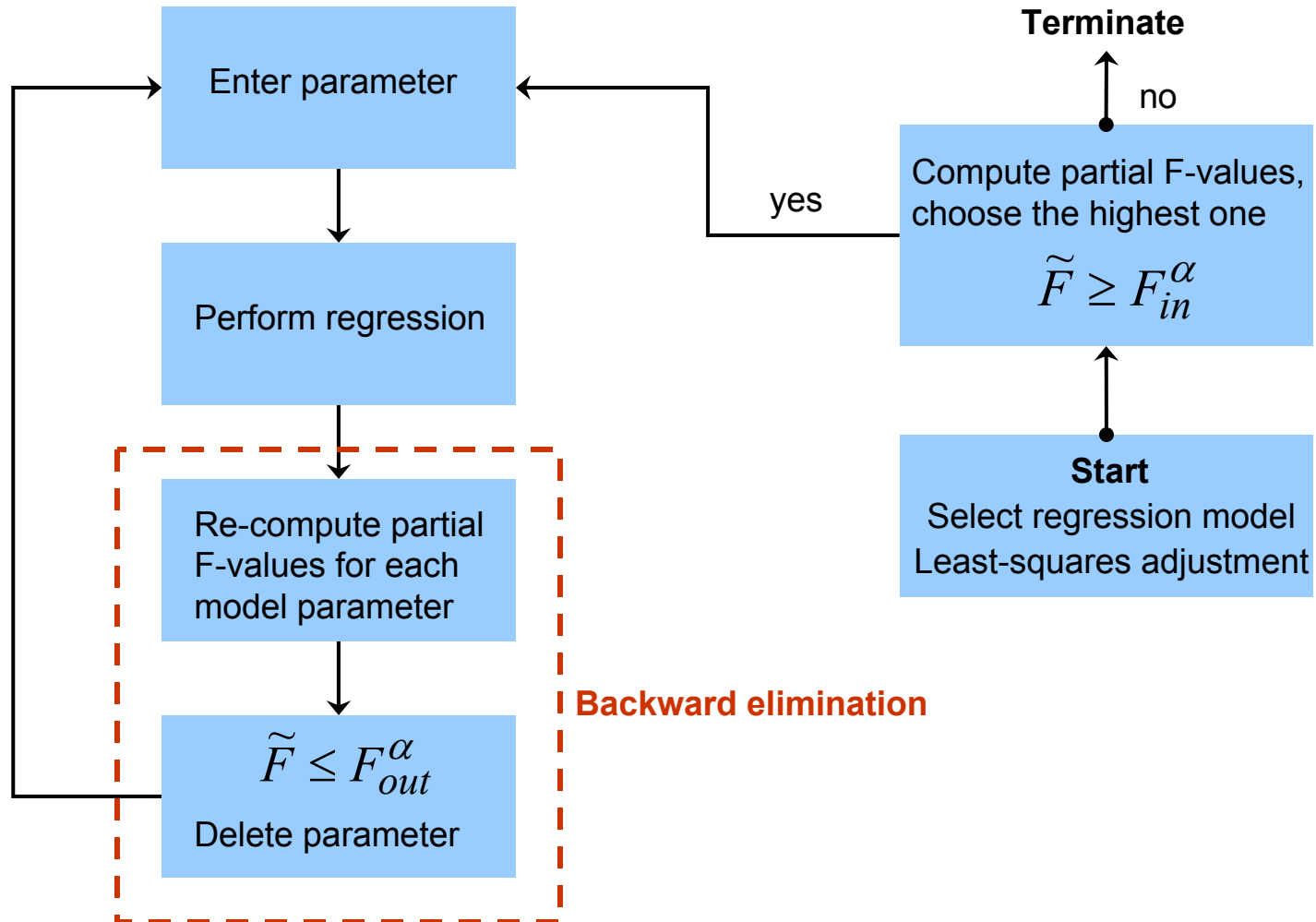
Forward Selection Procedure

- Start with simple model
- Add parameter with the highest coefficient of determination (or partial F-value)

Stepwise Procedure

- Combination of backward elimination and forward selection procedures
- Starts with no parameters and selects parameters one-by-one (or several)
- After inclusion, examine every parameter for significance (partial F-test)

Stepwise Procedure



Testing Parameter Significance

- Statistical tests are more powerful in pointing out inappropriate models rather than establishing model validity
- Test if a set of parameters in the model is significant or not:

$$x = \begin{bmatrix} x_{(I)} \\ x_I \end{bmatrix}$$

I ... set of parameters tested

(I) ... remaining parameters (complement)

hypothesis

$$H_0 : x_I = 0 \quad \text{vs} \quad H_a : x_I \neq 0$$

test statistic

$$\tilde{F} = \frac{\hat{x}_I Q_{\hat{x}_I}^{-1} \hat{x}_I}{k \hat{\sigma}^2}$$

k number of 'tested' terms

$Q_{\hat{x}_I}$ submatrix of $Q = N^{-1}$

criteria

$$\tilde{F} \leq F_{k,f}^{\alpha} \quad H_0 \text{ accepted } \checkmark$$

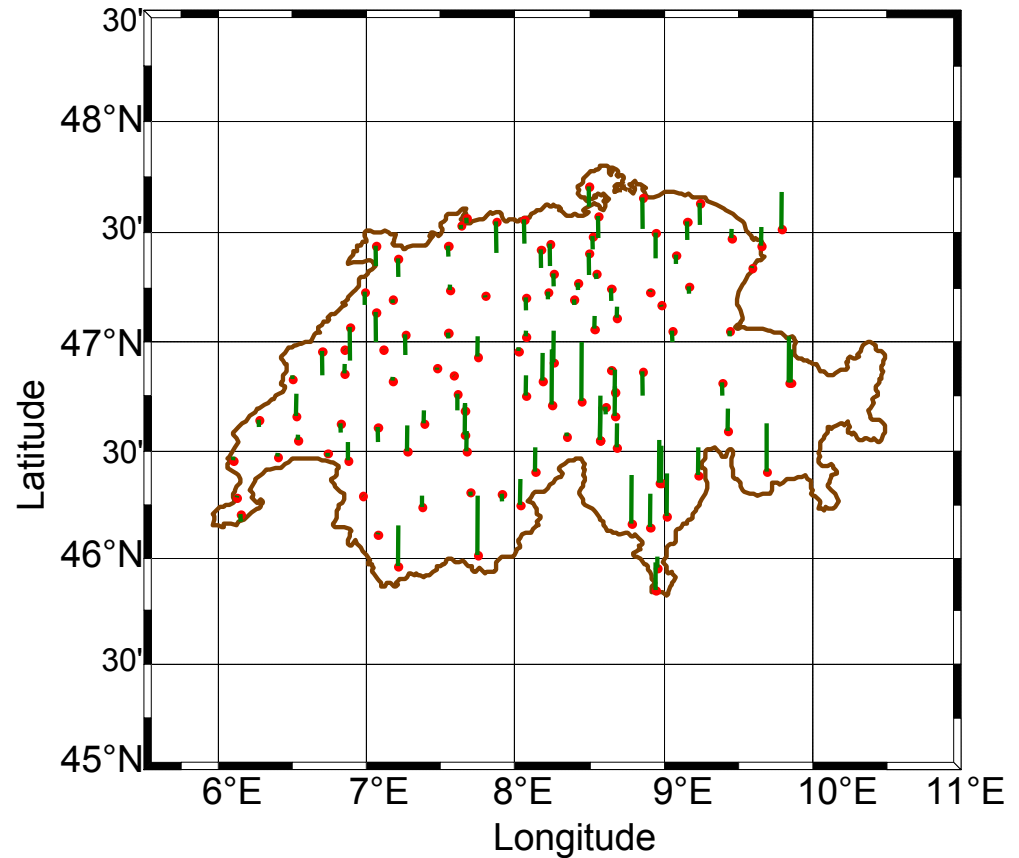
Examples - Switzerland

- 111 stations in **Switzerland**
- 343 km × 212 km region
- Form 'residuals':

$$\ell_i = h_i - H_i - N_i$$

Statistics of residuals before fit

min	-4.9 cm
max	19 cm
mean	1.1 cm
std	3.8 cm
rms	3.9 cm



GPS on Benchmarks (and residuals)

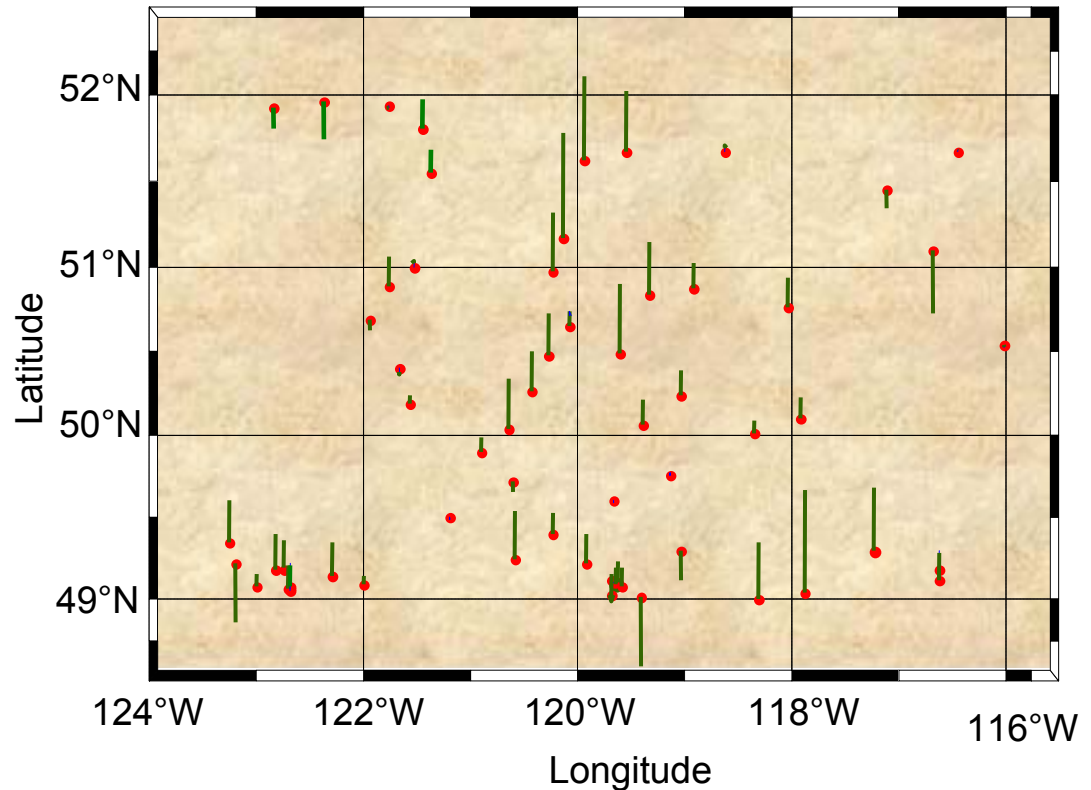
Examples - Canada

- 63 stations in **Southern British Columbia & Alberta**
- 495 km × 334 km region
- Form 'residuals':

$$\ell_i = h_i - H_i - N_i$$

Stats of residuals before fit

min	-17.1 cm
max	25.2 cm
mean	4.5 cm
std	8.1 cm
rms	9.3 cm



GPS on Benchmarks (and residuals)

Examples of Analytical Models

Nested bilinear polynomial series

$$1 \quad d\varphi \quad d\lambda \quad d\varphi d\lambda \quad d\varphi^2 \quad d\lambda^2 \quad d\varphi^2 d\lambda \quad d\varphi d\lambda^2 \quad d\varphi^3 \quad d\lambda^3 \quad d\varphi^2 d\lambda^2 \quad d\varphi^3 d\lambda \quad d\varphi d\lambda^3 \quad d\varphi^4 \quad d\lambda^4$$

Classic trigonometric-based polynomial fits

$$1 \quad \cos \varphi \cos \lambda \quad \cos \varphi \sin \lambda \quad \sin \varphi$$

$$1 \quad \cos \varphi \cos \lambda \quad \cos \varphi \sin \lambda \quad \sin \varphi \quad \sin^2 \varphi$$

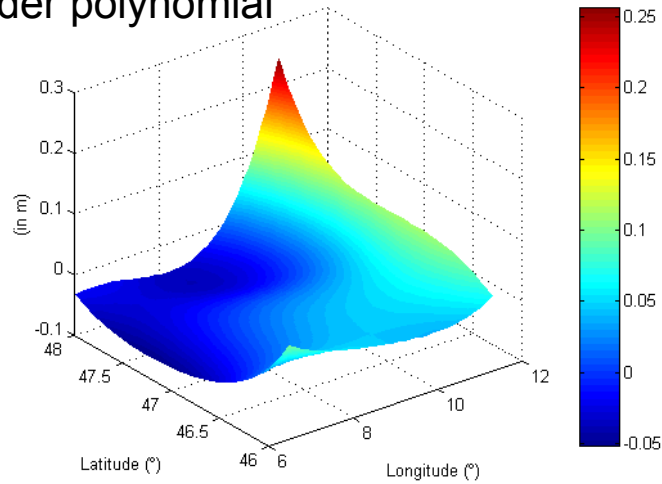
Differential similarity transformation

$$\cos \varphi \cos \lambda \quad \cos \varphi \sin \lambda \quad \sin \varphi \quad \frac{\sin \varphi \cos \varphi \sin \lambda}{W} \quad \frac{\sin \varphi \cos \varphi \cos \lambda}{W} \quad \frac{1 - f^2 \sin^2 \varphi}{W} \quad \frac{\sin^2 \varphi}{W}$$

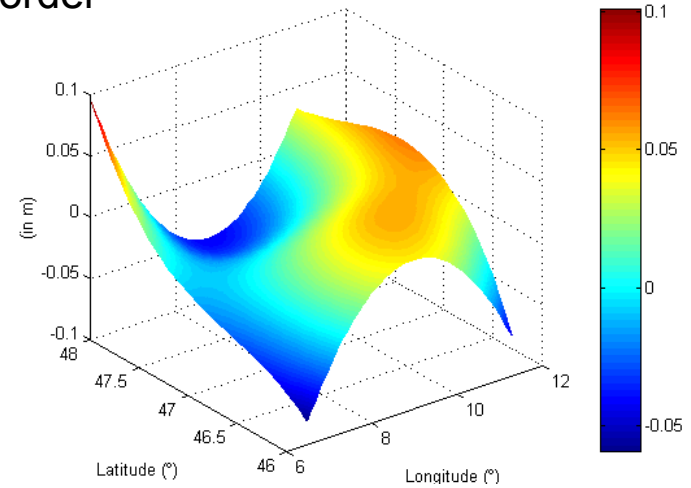
$$\text{where, } W = \sqrt{1 - e^2 \sin^2 \varphi}$$

Analytical Models

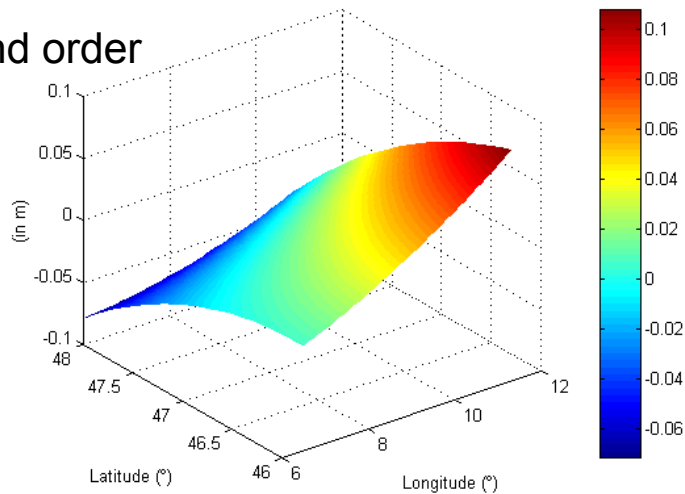
4th order polynomial



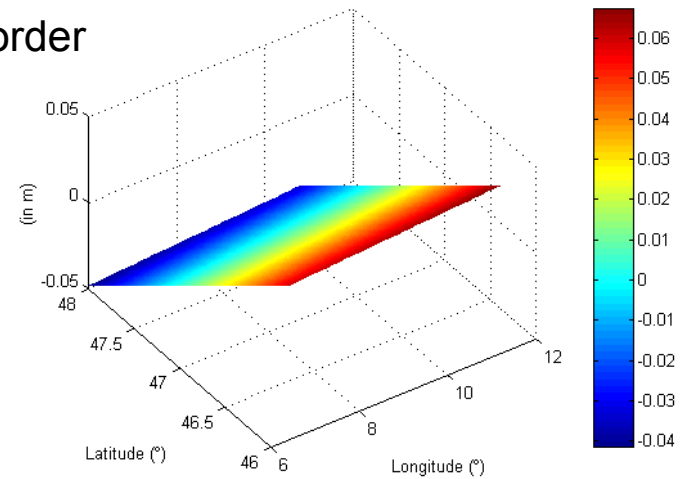
3rd order



2nd order

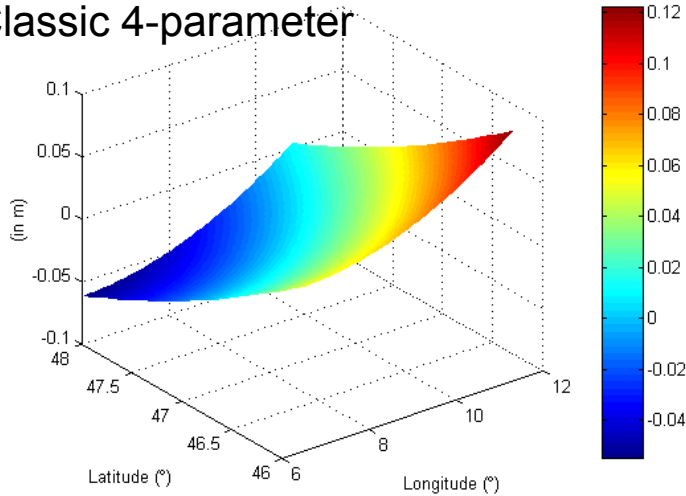


1st order

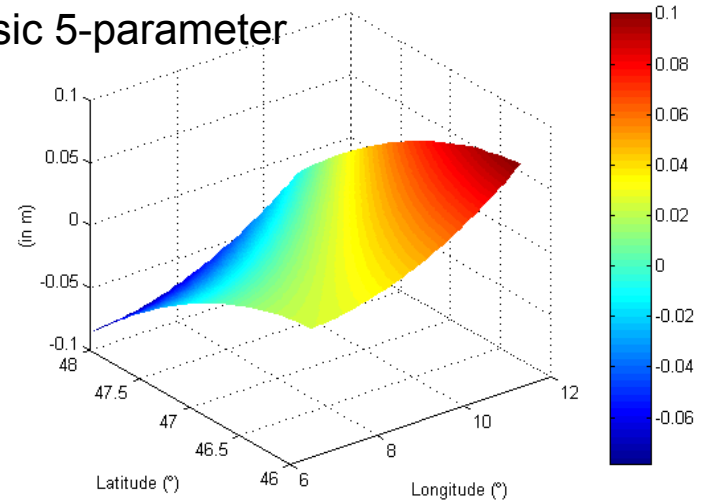


More Analytical Models

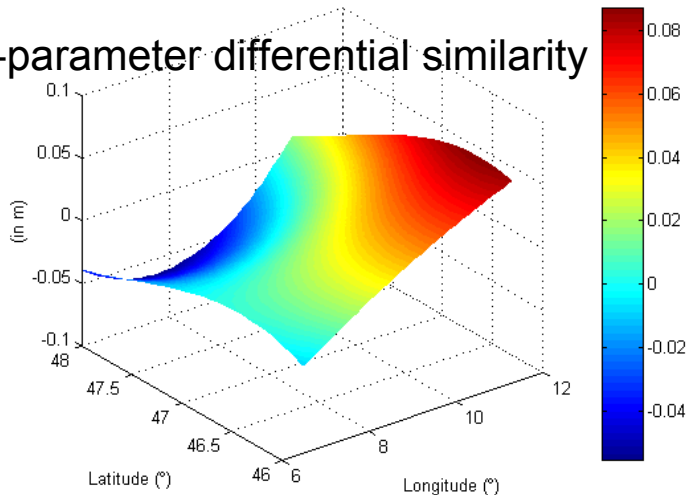
Classic 4-parameter



Classic 5-parameter



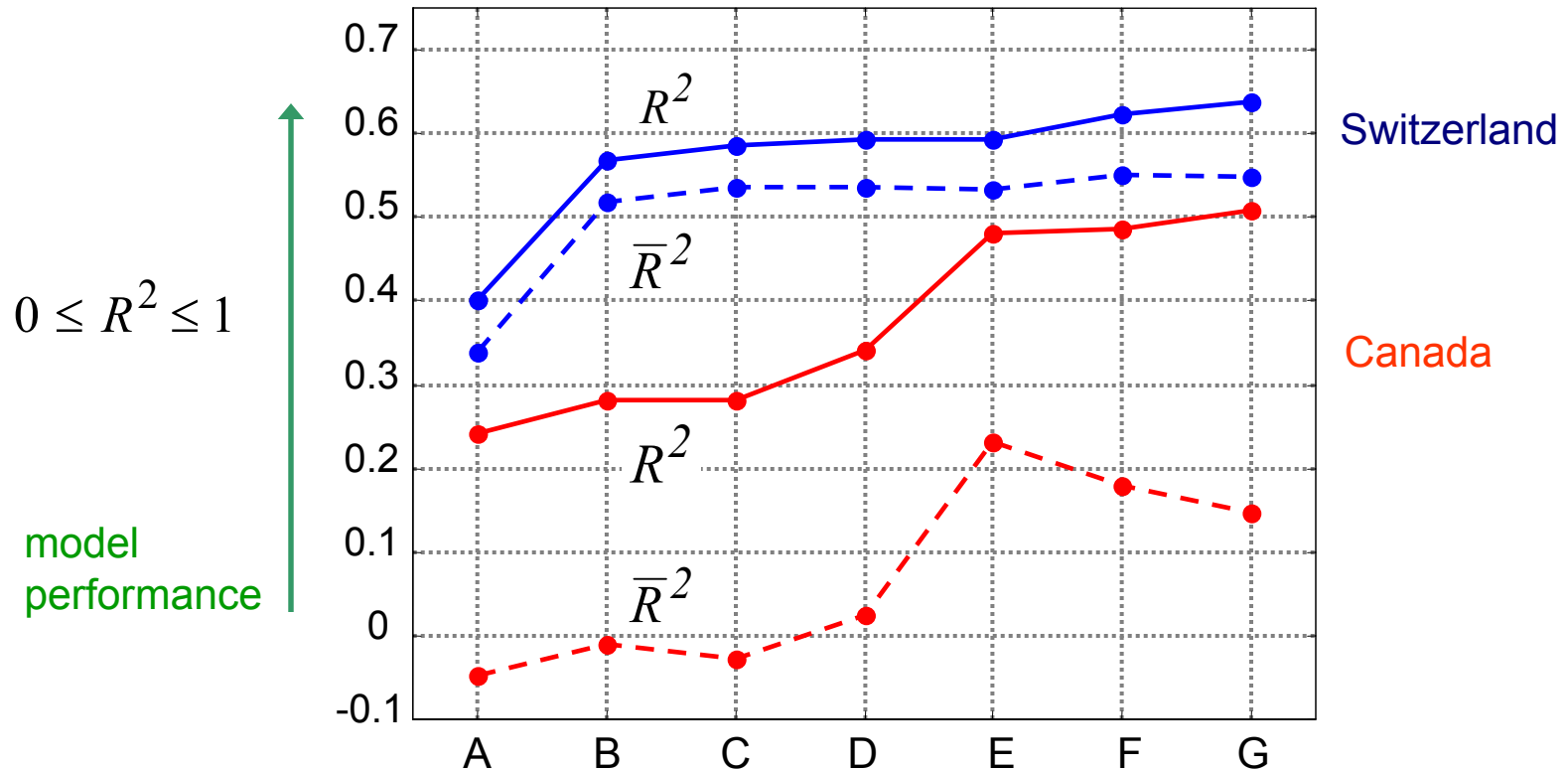
7-parameter differential similarity



Notes

- all values shown in m
- GPS BMs in Switzerland used
- Full models shown (no parameters omitted)

Example - Coefficient of Determination



A 1st order polynomial

B Classic 4-parameter

C Classic 5-parameter

D 2nd order polynomial

E Differential Similarity

F 3rd order polynomial

G 4th order polynomial

Empirical Testing (including cross validation)

Conclusions

Residuals after fit

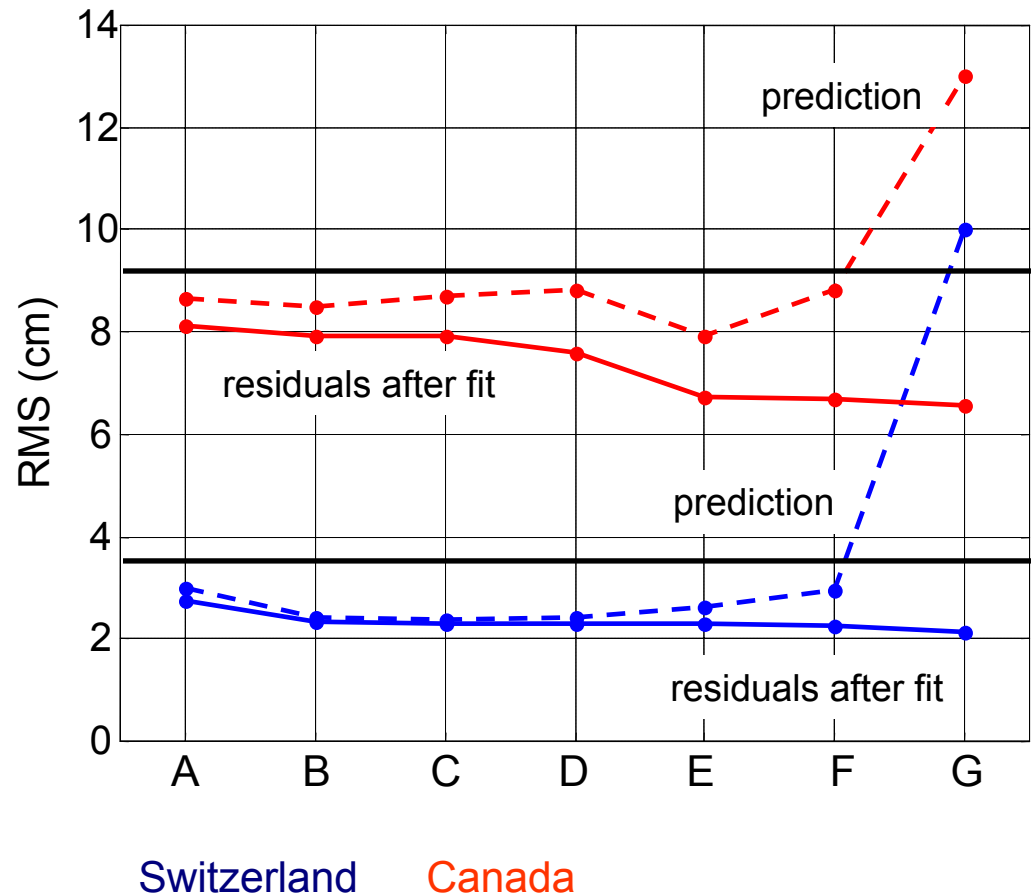
→ 4th order polynomial

Prediction (external test)

→ Any model except 4th order polynomial

Not enough of a difference between models to justify statistical parameter significance testing

→ use lowest order model



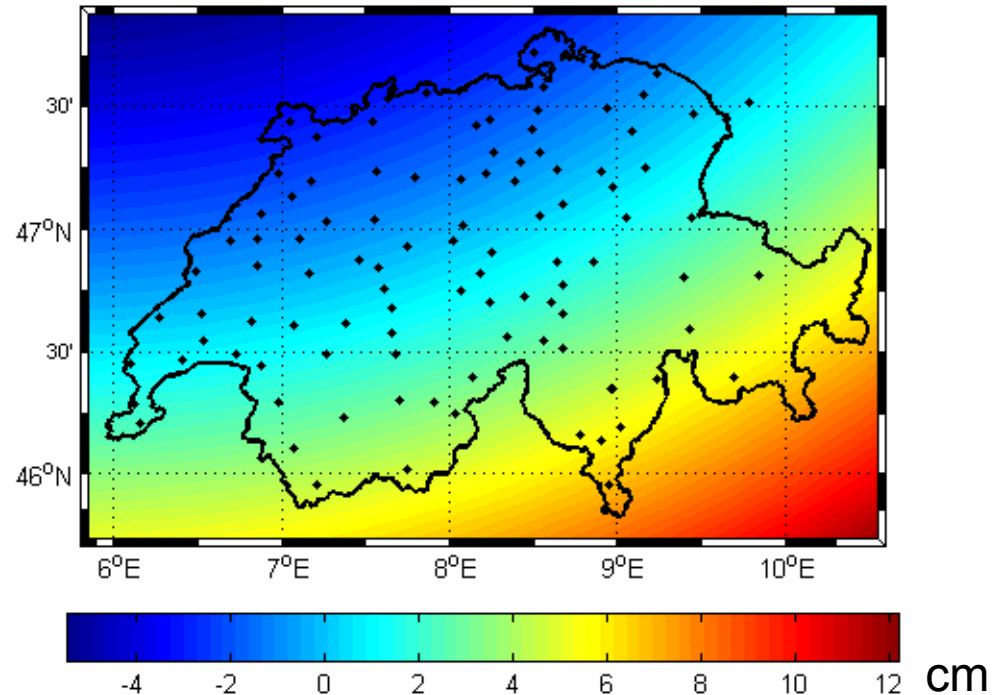
Results - Switzerland

Classic 4-parameter fit

$$I \cos \varphi \cos \lambda \quad \cos \varphi \sin \lambda \quad \sin \varphi$$

Selection criteria

R^2	0.5668
\bar{R}^2	0.5181
$\sqrt{\hat{v}^T \hat{v}}$	24.5 cm
condition number	2.77×10^7
rms after fit	2.4 cm
rms (prediction)	2.4 cm



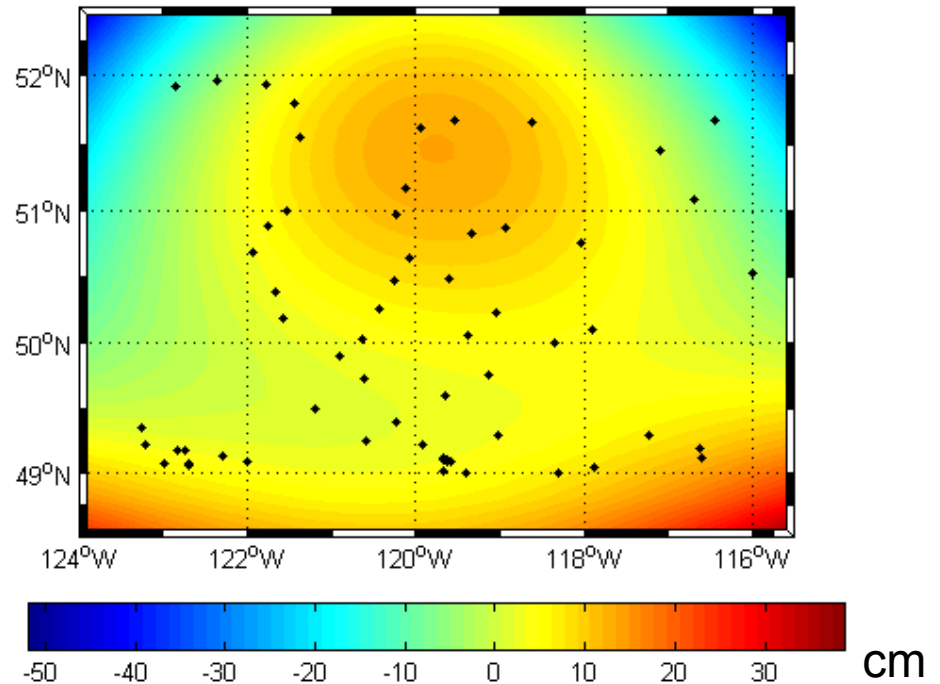
Results - Canada

Differential Similarity Fit (7-parameters)

$$\cos \varphi \cos \lambda \quad \cos \varphi \sin \lambda \quad \sin \varphi \quad \frac{\sin \varphi \cos \varphi \sin \lambda}{W} \quad \frac{\sin \varphi \cos \varphi \cos \lambda}{W} \quad \frac{1 - f^2 \sin^2 \varphi}{W} \quad \frac{\sin^2 \varphi}{W}$$

Selection criteria

R^2	0.4805
\bar{R}^2	0.2311
$\sqrt{\hat{v}^T \hat{v}}$	53 cm
condition number	1.52×10^{12}
rms after fit	6.7 cm
rms (prediction)	7.9 cm



Summary

- **Semi-automated procedure** for **comparing parametric surface models** and **assessing model performance** was presented
- ***Semi***
 - no unique straightforward solution
 - some user intervention required
- In most cases, the best test is cross-validation (prediction)
 - independent 'external' test
 - depends on quality of data
- When model parameters are highly correlated (as is the case with polynomial regression), statistical testing may not be conclusive
- Use orthogonal polynomials to eliminate problems with high correlation between parameters (i.e. Fourier Series)
- Procedure should include a **combination** of empirical **and** statistical testing